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REUSE OF WASTE OIL AT ARMY INSTALLATIONS(U)  
CONSTRUCTION ENGINEERING RESEARCH LAB (ARMY) CHAMPAIGN  
IL L C CHICOINE ET AL. SEP 82 CERL-TR-N-135

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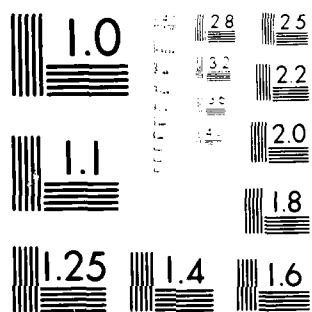
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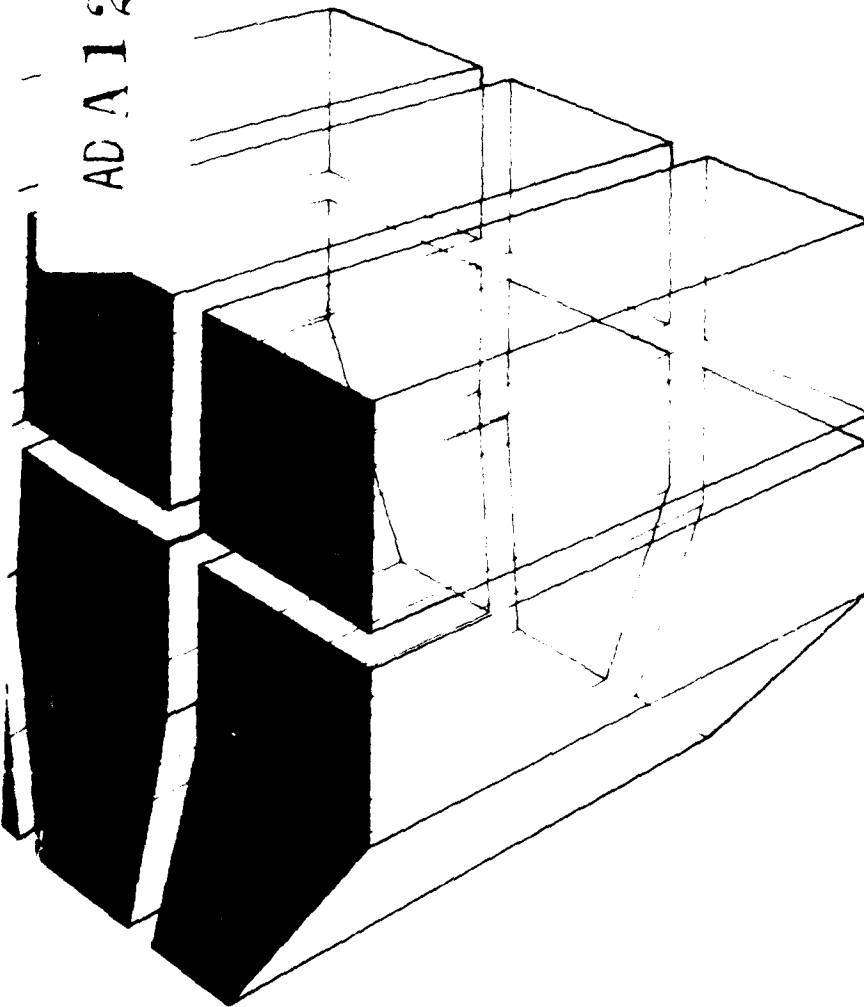


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TECHNICAL REPORT N-135  
September 1982  
Hazardous/Toxic Waste Control

REUSE OF WASTE OIL AT ARMY INSTALLATIONS

AD A123097



by  
L. C. Chicoine  
G. L. Gerdes  
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|--|-------------------------------------|--|
| 1. REPORT NUMBER<br>CERL-TR-N-135  | 2. GOVT ACCESSION NO.<br>[REDACTED] | 3. RECIPIENT'S CATALOG NUMBER<br>AD-7123097  |
| 4. TITLE (and Subtitle)<br>REUSE OF WASTE OIL AT ARMY INSTALLATIONS  |                                     | 5. TYPE OF REPORT & PERIOD COVERED<br>FINAL  |
|  |                                     | 6. PERFORMING ORG. REPORT NUMBER   |
| 7. AUTHOR(s)<br>L. V. Chicoine<br>G. L. Gerdes<br>B. A. Donahue  |                                     | 8. CONTRACT OR GRANT NUMBER(s)   |
| 9. PERFORMING ORGANIZATION NAME AND ADDRESS<br>U.S. ARMY<br>CONSTRUCTION ENGINEERING RESEARCH LABORATORY<br>P.O. BOX 4005, CHAMPAIGN, IL 61820   |                                     | 10. PROGRAM ELEMENT PROJECT TASK<br>AREA & WORK UNIT NUMBERS<br>4A762720A896-A-032 |
| 11. CONTROLLING OFFICE NAME AND ADDRESS  |                                     | 12. REPORT DATE<br>September 1982  |
|  |                                     | 13. NUMBER OF PAGES<br>43  |
| 14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)  |                                     | 15. SECURITY CLASS. of this report<br>Unclassified                                 |
|  |                                     | 15a. DECLASSIFICATION DOWNGRADING<br>SCHEDULE                                      |
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| 19. KEY WORDS (Continue on reverse side if necessary and identify by block number)<br><br>waste recycling<br>oil wastes  |                                     |  |
| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number)<br><br>Typical Army installations produce large amounts of waste oil - up to 250,000 gal annually. In response to the growing need for energy conservation, Army policy requires that these installations reuse oil whenever possible. The objective of this report is to analyze the economics of waste oil reuse, and to examine the environmental aspects of used oil management. |                                     |  |

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Regulatory requirements dealing with waste oil reuse were reviewed, and personnel with Army agencies, the General Accounting Office, the Environmental Protection Agency, State agencies, and private industry were interviewed. Waste oil from three Army installations was analyzed.

Three options for reusing waste oil were assessed: selling the oil to a re-refinery, burning it as a boiler fuel, and recycling it in a closed loop agreement with a re-refiner. The closed loop recycling option appears to be most economical.

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## FOREWORD

This report was prepared for the Directorate of Military Programs, Office of the Chief of Engineers (OCE), under Project 4A762720A896, "Environmental Quality for Construction and Operation of Military Facilities"; Task Area A, "Installation Environmental Management Strategy"; Work Unit 032, "Hazardous/Toxic Waste Control." The research was performed by the Environmental Division (EN) of the U.S. Army Construction Engineering Research Laboratory (CERL). Principal Investigator was Mr. B. A. Donahue. The OCE technical monitors were Mr. R. Newsome and Mr. F. Bizzoco. Dr. R. K. Jain is Chief of EN.

Special acknowledgement is given to Dr. R. Vogel, coordinator of the chemical analysis, and Mr. A. Miekowski, chemist, for their work in the oil characterization.

COL Louis J. Circeo is Commander and Director of CERL, and Dr. L. R. Shaffer is Technical Director.



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## REUSE OF WASTE OIL AT ARMY INSTALLATIONS

### 1 INTRODUCTION

#### Background

Typical Army installations produce large amounts of waste oil—up to 250,000 gal annually. Recent emphasis on energy conservation and regulations concerning hazardous wastes have caused the Army to consider reusing its waste oil.<sup>1</sup> The Office of the Chief of Engineers (OCE) asked the U.S. Army Construction Engineering Research Laboratory (CERL) to assess waste oil handling and reuse for Directorate of Facility Engineers (DFAE) and Defense Property Disposal Office (DPDO) personnel.

#### Objective

The objectives of this research were: (1) to analyze the economics of waste oil reuse, and (2) to examine the environmental aspects of used oil management.

#### Approach

The state of the art of waste oil management was surveyed through a literature search and contacts with personnel at various Governmental and private agencies. Representatives from Army commands, Army installations, the General Accounting Office (GAO), the U.S. Environmental Protection Agency (EPA), State agencies, and re-refiners were interviewed. Waste oil samples from three installations were analyzed to see how the characteristics of Army waste oil affect reuse options (Chapters 2 and 3).

From this information, CERL assessed the three handling and reuse alternatives that are most appropriate for the Army: (1) selling the oil to a re-refinery, (2) burning it as a boiler fuel, and (3) recycling it in a closed loop agreement with a re-refiner (Chapter 4).

#### Mode of Technology Transfer

It is recommended that the information in this report impact on the Army Energy Plan and AR 200-1.

<sup>1</sup>Army Energy Plan (Headquarters, Department of the Army, 1978).

## 2 REGULATIONS AFFECTING WASTE OIL REUSE

#### Federal Water Pollution Control Act Amendments of 1972

One of the first and most important pieces of environmental legislation of the 1970s was the Federal Water Pollution Control Act Amendments of 1972. The purpose of this legislation was to reduce and eventually eliminate the discharge of pollutants into the nation's navigable waters. Discharging toxic pollutants in harmful amounts was prohibited immediately. One concern of Congress was the degradation of the environment caused by the improper disposal of waste oil. The EPA was directed to conduct a study of:

1. The generation of used engine, machine, cooling and similar waste oil, including quantities, quality, present collection and disposal practices, and alternate uses.
2. The long-term, chronic biological effects of the disposal of waste oil.
3. The potential market for waste oils. The following issues were to be considered: the economic and legal factors relating to the sale of products made from such oils, the level of subsidy needed to encourage public and private nonprofit agencies to buy the products, and the possibility of Federal procurement of these products.

The result of this work was the EPA's *Waste Oil Study*.<sup>2</sup>

#### PL 94-163

To reduce energy demand and provide emergency conservation measures, the Congress passed the Energy Policy and Conservation Act (PL 94-163) in December 1975. The authors of this bill recognized used crankcase oil as a valuable, reusable resource and devoted a section of the law to policy on recycled oil. Section 383 of PL 94-163 was intended:

1. To encourage the recycling of used oil
2. To promote the use of recycled oil

<sup>2</sup>Waste Oil Study—A Report to the Congress, PB257693 (Environmental Protection Agency [EPA], April 1974).

3. To reduce consumption of new oil by promoting increased use of recycled oil

4. To reduce environmental hazards and wasteful practices associated with the disposal of used oil.

In addition, PL 94-163 directed the National Bureau of Standards (NBS) to "develop test procedures to determine substantial equivalency of re-refined or otherwise processed used oils or blend of new and used oil for a particular end use." Test procedures developed by the Bureau for burner fuel were published in 1980.<sup>1</sup>

PL 94-163 also directed the Federal Trade Commission, after reviewing the Bureau's test procedures, to prescribe labeling standards for recycled oil containers. For containers of new oil, used oil, and recycled oil, the EPA was directed to establish labeling standards concerning the proper disposal of oil after use. Also, all Federal agencies were to revise policies to encourage procurement of recycled oil when available at competitive prices for the same use as new oil.

Finally, Federal agencies were to inform Federal, State, and private sector employees about the need to use recycled oil to conserve new oil and to prevent environmental hazards associated with improper oil disposal.

#### **Resource Conservation and Recovery Act**

In 1976, the Solid Waste Disposal Act (42 USC 3251) was amended by the Resource Conservation and Recovery Act (RCRA) PL 94-580. The revised law offers technical and financial assistance in developing facilities for and managing not only recovery of energy, but also safe disposal or recovery of discarded materials. The law also regulates the management of hazardous wastes. Section 3001 of RCRA requires the EPA to issue criteria for identifying hazardous wastes and for categorizing those subject to RCRA's subtitle (c). When characterizing a hazardous waste, the EPA must consider factors such as toxicity, persistence, degradability, potential for accumulation in tissue, flammability, and corrosiveness.

The hazardous waste regulations were issued in May 1980 (40 CFR Part 260), but used oil was not

specifically mentioned, although it was in the proposed regulations. Nonetheless, CERL believes that used crankcase oil would qualify as a hazardous waste if it failed the toxicity test specified in the regulations.

#### **Used Oil Recycling Act**

The Used Oil Recycling Act of 1980 (PL 96-463) amended the Solid Waste Disposal Act to specifically include used oil. This law is described fully here because it is directly relevant to Army recycling policy.

Section 2 of the Act lists Congressional findings which reflect an increasingly favorable attitude toward used oil. Congress found that

1. Used oil is a valuable source of scarce energy and materials.

2. Technology exists to re-refine, reprocess, reclaim, and otherwise recycle used oil.

3. Used oil constitutes a threat to public health and the environment when reused or disposed of improperly. Therefore, it is in the national interest to recycle used oil in order to protect public health and the environment, and to conserve energy and materials.

Section 4 of the Act deals with labeling requirements for new and used oil containers. Part (c) effectively repeals the rule which requires used oil containers to bear a label indicating that the oil was made from used or recycled oil. It was thought that this notice implied that the product was inferior.

Section 5 (b) amends Section 4008 of the Solid Waste Disposal Act by adding a subsection providing financial assistance to States for oil recycling programs. To carry out the provisions of Section 5, Congress allocated \$5 million each for fiscal years 1982 and 1983. None of the funds may be used for construction, land acquisition, or equipment.

Section 6 of PL 96-463 amends Section 4008 of the Solid Waste Disposal Act by authorizing the EPA to provide technical assistance to States which have to address economic and institutional problems with recycling used oil.

Section 7 amends subtitle (C) of the Solid Waste Disposal Act and directs the EPA to issue regulations on performance standards and other requirements necessary to protect public health and the environment from the hazards associated with recycled oil.

<sup>1</sup>D. A. Becker and J. J. Cometord, *Recycled Oil Program: Phase I Test Procedures for Recycled Oil Used as Burner Fuel*, Technical Note 1130 (National Bureau of Standards [NBS], August 1980).

Within 90 days after the enactment of PL 96-463 (or by 15 January 1981) the EPA was required by Section 8 to decide whether subsections 3001 (a) and (b) of the Solid Waste Disposal Act are applicable to used oil (i.e., is it a hazardous waste), and to report the decision and relevant data to Congress. The EPA was not to discourage the recycling and reuse of used oil when making this decision.

Finally, Section 9 requires the Administrator of the EPA, the Secretary of Energy, the Federal Trade Commission, and the Secretary of Commerce to study the environmental problems associated with the improper disposal or reuse of used oil, collection of used oil before recycling, supply and demand in the used oil industry, and energy savings associated with re-refining and recycling used oil.

#### DOD Policy

The Department of Defense (DOD) recognized the importance of proper management of waste oil before the Used Oil Recycling Act was passed. "Oil Recycling and Reuse Policy" is the subject of a 1979 DOD memorandum.<sup>4</sup> This document emphasizes re-refining waste oil and, if more economical, burning waste oil as a fuel.

A subsequent memorandum directs DOD to "establish a priority system to maximize the sale of used lube oil to re-refiners, reprocessors, brokers for re-refiners/reprocessors, and energy converters, and to purchase re-refined lube oil from industry through closed loop or stock, store, and issue systems."<sup>5</sup>

The most significant change in DOD regulations to promote the purchase of re-refined oil was the revision of MIL-L-46152, "Lubricating Oil, Internal Combustion Engine, Administrative Service," the specification qualifying engine lubricating oil for administrative service vehicles. The revision to MIL-L-46152A (23 January 1980) and then to MIL-L-46152B (26 January 1981) allows used oil as a feed stock. Previously, buying re-refined oil had been prohibited. MIL-L-2014,

"Lubricating Oil, Internal Combustion Engine, Tactical Service," is also being changed to allow used oil as a feed stock.

### 3 CURRENT WASTE OIL MANAGEMENT

#### Sources

Waste oil at Army installations comes from the maintenance of tactical, support, and facility engineering vehicles. Crankcase oils, transmission oils, final drive oils, and hydraulic fluids are removed periodically from these vehicles at the maintenance facilities.

Tactical vehicles provide most of the Army's used oil, as indicated by the crankcase and transmission capacities shown in Tables 1 and 2. Oil is changed about twice a year for tanks and other tracked vehicles, and once a year for armored personnel carriers. The oil in wheeled vehicles is changed twice a year, unless it is done according to mileage.<sup>6</sup>

#### Storage

Waste oil is stored in three places before it is finally disposed of: the container used to catch the oil when it is drained from a crankcase, a pod or underground storage tank to hold oil changes from one or more maintenance units, and central storage tanks serving the entire installation. The oil is usually hand-carried in its collection container from the motor pool to the maintenance unit's storage tank. Each unit's oil is usually picked up by a contractor and transferred to the central storage tank; however, at some installations the oil is hauled to the central storage area by the units. If the contractor collecting the oil from the units is also hauling the oil to a waste oil processing facility, then there probably will not be a central storage tank on the installation.

#### Quantity

The Defense General Supply Center reported that 3,329,842 gal of new crankcase oil were shipped to Army facilities between June 1979 and June 1980. Of this amount, 315,105 gal were to be used in administrative vehicles. These oils were required to meet

<sup>4</sup>"Oil Recycling and Reuse Policy." Memorandum for the Secretaries of the Military Departments, the Directors Defense Agencies (Assistant Secretary of Defense [Manpower, Reserve Affairs, and Logistics]), June 4, 1979).

<sup>5</sup>"Defense Environmental Actions for 1981." Defense Environmental Quality Program Policy Memorandum No. 81-1 (Assistant Secretary of Defense [Manpower, Reserve Affairs, and Logistics]), 12 January 1981).

<sup>6</sup>R. Fileccia, J. Benson, and J. Matherly, *In Hardstand Tactical Vehicle Maintenance Facilities: Concept Design and Preliminary Recommendations for Wastewater Treatment*. Interim Report N-67/ADA067985 (U.S. Army Construction Engineering Research Laboratory [CFRL], 1979), pp 10, 11.

**Table 1**  
**Characteristics of Various Types of Track-Laying Vehicles**

| Designation | General Description                        | Crankcase<br>Capacity,<br>Qt | Transmission<br>Capacity,<br>Qt |
|-------------|--|------------------------------|---------------------------------|
| M48A1       | Tank, combat, 90 mm                        | 72                           | 92                              |
| M48A2/A2C   | Tank, combat, 90 mm                        | 64                           | 92                              |
| M48A3       | Tank, combat, 90 mm                        | 48                           | 76                              |
| M60/60A1    | Tank, combat, 105 mm                       | 48                           | 76                              |
| M107        | Gun, self-prop, 175 mm                     | 26                           | 57+                             |
| M110        | Howitzer, self-prop, 8-in.                 | 26                           | 57+                             |
| M109        | Howitzer, self-prop, 155 mm                | 28                           | 52+                             |
| M108        | Howitzer, self-prop, 155 mm                | 26                           | 58+                             |
| M42/42A1    | Gun, Anti-aircraft                         | 44                           | 44                              |
| M56         | Gun, self-prop, 90 mm                      | 11                           | 15                              |
| M53         | Gun, self-prop, 155 mm                     | 104                          | 96+                             |
| M55         | Howitzer, self-prop, 8-in.                 | 64                           | 72+                             |
| M37         | Howitzer, self-prop, 105 mm                | 16                           | 30+                             |
| M52/52A1    | Howitzer, self-prop, 105 mm                | 44                           | 49                              |
| M44/44A1    | Howitzer, self-prop, 155 mm                | 44                           | 70                              |
| M84         | Mortar, self-prop, 107 mm                  | 22                           | 45                              |
| 53          | Vehicle, combat engr, 165 mm               | NA                           | 688                             |
| M5-M5A4     | Tractor, high speed                        | 22                           | 48                              |
| M8A1 - M8A2 | Tractor, high speed                        | 44                           | 72                              |
| M6          | Bulldozer, tank mounted                    | 64                           | 80+                             |
| M8          | Bulldozer, tank mounted                    | 72                           | 92                              |
| M9          | Bulldozer, tank mounted                    | 48                           | 76                              |
| M578        | Recovery vehicle                           | 26                           | NA                              |
| M88         | Recovery vehicle                           | 64                           | 72                              |
| M113        | Armored personnel carrier                  | 10                           | 16                              |
| M577-M577A1 | Armored personnel carrier,<br>command post | 12<br>18                     | 12                              |

MIL-L-46152 specifications. In addition, 2,924,737 gal. shipped for use in tactical vehicles, had to qualify under MIL-L-2104.

The literature commonly assumes that 50 percent of the crankcase oil is lost during use, disposed of with the filter cartridge, or spilled.<sup>7</sup> If 50 percent of the

<sup>7</sup>H. B. Kaufman, "EPA Activities in Waste Oil Management," *Proceedings of a Workshop on Measurements and Standards for Recycled Oil-II*, Gaithersburg, Maryland, National Bureau of Standards, 1977 (NBS Special Publication 556, 1979), p. 201.

Army's oil is indeed lost, then 1,600,000 gal of used oil is produced each year. Some Army facilities and their approximate rates of used oil production are listed in Table 3. Table 4 is an example of generation rates from the maintenance units at Fort Lewis, WA.<sup>8</sup>

<sup>8</sup>R. Fileccia, J. Benson, and J. Matherly, *In-Hardstand Tactical Vehicle Maintenance Facilities Concept Design and Preliminary Recommendations for Wastewater Treatment*, Interim Report N-67/ADA067985 (CFRL, 1979).

**Table 2**  
**Characteristics of Various Types of Wheeled Vehicles**

| Designation                                   | General Description      | Crankcase Capacity Qt |
|---|--------------------------|-----------------------|
| M170  | 1/4-ton ambulance        | 5.5                   |
| M43 - M43B1                                   | 3/4-ton ambulance        | 5                     |
| M44,M45,M46,<br>M46C,M58,M133,<br>M207,M207C  | 2-1/2-ton truck chassis  | 9                     |
| M34,M36,M36C                                  | 2-1/2-ton truck chassis  | 18                    |
| M40,M40C,M61<br>M63,M63C,M139,<br>M139C,M139D | 5-ton cargo              | 9                     |
| M135,M211,M35<br>M54,M2,M55                   | 2-1/2-ton cargo truck    | 11                    |
| M125  | 10-ton cargo truck       | 22                    |
| M342  | 2-1/2-ton cargo, dump    | 10.5                  |
| M51   | 5-ton dump               | 22                    |
| M49,M49C                                      | 2-1/2-ton gasoline       | 9                     |
| M217,M217C                                    | 2-1/2-ton fuel servicing | 9                     |
| M150,M222                                     | 2-1/2-ton water          | 9                     |
| M48,M221,M275                                 | 2-1/2-ton truck tractor  | 9                     |
| M52,M52A1                                     | 5-ton truck tractor      | 22                    |
| M123,M123C,M123D                              | 10-ton truck tractor     | 22                    |
| M246  | 5-ton wrecker            | 22                    |
| M38,M38A1,M38A1C                              | 1/4-ton utility          | 4                     |
| M151  | 1/4-ton utility          | 4                     |
| M108,M60                                      | 2-1/2-ton wrecker        | 9                     |
| M62,M62F1                                     | 5-ton wrecker            | 18                    |
| M512,M512C,M512D<br>M5121,M512G               | 2-1/2-ton shop vans      | 9                     |

**Table 3**  
**Used Crankcase Oil Production Rates  
of Some Army Facilities**

| Installation             | Gal/Yr  |
|--------------------------|---------|
| Fort Hood, TX            | 256,596 |
| Fort Polk, LA            | 255,364 |
| Toelle Army Depot, UT    | 125,948 |
| Stewart/Hunter AAF, TX   | 142,236 |
| Red River Army Depot, TX | 122,124 |
| Anniston Army Depot, AL  | 118,000 |
| Fort Bragg, NC           | 108,400 |
| Fort Carson, CO          | 90,400  |

### Quality

Before any oil recycling or reuse process is selected, the contaminants in the used oil must be identified and the contaminants' sources examined. Generally, contaminants are classified as metals, water, sediment, and ash. Table 5 gives the general characteristics of used oil. Table 6 lists typical additives and contaminants in used oil.

CERL conducted a limited characterization study to see if the Army's waste oil is similar to that discussed in the literature. Sampling was done at Fort Eustis, Fort Bragg, and Fort Benning; these installations were chosen because they are representative of the average producers of Army waste oil. All three installations have central storage tanks from which waste oil samples were taken. The results of CERL's analyses are shown in Table 7. Although time and funding restrictions prevented a more comprehensive analysis of the samples, the parameters considered most important for processing the oil or using it as boiler fuel were included.

### Sources of Contaminants in Used Oil

Commercial basestocks contain only very small concentrations of metals, so these contaminants are introduced to oil as additives, or from wear, corrosion, or combustion.<sup>9</sup> Additives, which usually constitute 20 percent, by volume, of high grade crankcase oils, typically contain sodium, barium, calcium, zinc, and magnesium compounds.<sup>10</sup> Wear and corrosion processes contribute aluminum, copper, iron, silicon, and tin.<sup>11</sup> Combustion of leaded fuels in gasoline engines may cause the lead concentration in crankcase oils to increase by a factor of 10,000 to as much as 1:1.4 percent by weight.<sup>12</sup>

Of course, the metal profiles of gasoline engine and diesel engine crankcase oils differ; most significant is that used crankcase oil from diesel engines contains no

<sup>9</sup>T. D. Coyle and A. R. Siedle, "Metals in Oil: Occurrence and Significance for Reuse of Spent Automotive Lubricating Oils," *Proceedings of a Workshop on Measurements and Standards for Recycled Oil-II*, Gaithersburg, Maryland, National Bureau of Standards, 1977 (NBS Special Publication 556, 1979), p. 197.

<sup>10</sup>*Waste Oil Study: A Report to the Congress*, PB257693 (Environmental Protection Agency [EPA], April 1974), p. 16.

<sup>11</sup>*Waste Oil Study*, p. 16.

<sup>12</sup>Coyle and Siedle, p. 23.

**Table 4**  
**Estimated Waste Oil Generated Annually by Various Tactical Units**

| Unit Designation                     | Vehicle Counts |         | Estimated Waste Oil Generated,<br>Gal* |
|--------------------------------------|----------------|---------|--|
|                                      | Track          | Wheeled |  |
| Cavalry Squadron                     | 36             | 43      | 800                                    |
| Artillery Battalion<br>(BN) (mt div) | 0-5            | 91-111  | 400-900                                |
| Air Defense Artillery BN             | 44             | 115     | 900                                    |
| Military Police Group (GP)           |                | 54      | 100                                    |
| Ordnance CO                          | 2              | 46      | 400                                    |
| Transportation CO                    |                | 70-73   | 300-600                                |
| Adjutant General CO                  |                | 29      | 100                                    |
| Signal BN                            |                | 160-222 | 600                                    |
| Engineer BN                          | 12-18          | 214-213 | 800-1700                               |
| Military Intelligence GP             |                | 21      | 100                                    |
| Armored BN                           | 94             | 78      | 3400                                   |
| Mechanized Infantry BN               | 88             | 91      | 900                                    |
| Medical GP                           | 108            |         | 300                                    |
| Infantry BN                          |                | 116     | 300                                    |
| Supply & Transport CO                |                | 123     | 600                                    |
| Aviation BN                          |                | 46      | 200                                    |

\*Rounded to next highest 100 gal.

incremental lead from the combustion process.<sup>13</sup> This is an important consideration in the evaluation of reuse options discussed in Chapter 4. Additional metal contamination may occur during the collection, handling, and storage of the used oils. Table 5 lists some common metal contaminants and trace metals, and their concentration ranges in used oil.

During use, crankcase oil changes chemically and physically. Additives are consumed or undergo molecular change, and lead and wear metals accumulate as particulates. Organics are volatilized and inorganics are concentrated as oil losses occur.<sup>14</sup> Zinc dialkylidithio-

phosphate, an antiwear additive, is degraded to inorganic zinc-containing substances.<sup>15</sup> According to Coyle and Siedle, calcium dialkyl-naphthalene sulfonates are partially converted to inorganic calcium compounds and organic products. Magnesium and barium sulfonates may hydrolyze to produce their respective hydroxides.<sup>16</sup>

Organic bromine compounds are added to gasoline to scavenge lead as lead bromide. Coyle and Siedle suggest that some of the lead in oil from gasoline engines is present as lead dibromide. Lead is also thought to be present as lead salts and chlorides.<sup>17</sup>

<sup>13</sup>Waste Oil Preliminary Report to the Congress (Environmental Protection Agency, April 1973), as cited in T. D. Coyle and A. R. Siedle, "Metals in Oil: Occurrence and Significance for Reuse of Spent Automotive Lubricating Oils," *Proceedings of a Workshop on Measurements and Standards for Recycling Oil-II*, Gaithersburg, Maryland, National Bureau of Standards, 1977 (NBS Special Publication 556, 1979), p 197.

<sup>14</sup>Waste Oil Study, p 12

<sup>15</sup>C. Versino and C. DelSole, "Cromatografia S-Le Spettrofotometria IR di Oil Minerali Lubrificanti," *La Rivista dei Combustibili*, Vol 26, No. 321 (1972); C. Versino, A. Bacciorini, and C. DelSole, "Spettrofotometria IR di un Olio Minerale Lubrificanti Esausto," *La Rivista dei Combustibili*, Vol 26, No. 421 (1972), as cited in Coyle and Siedle, p 203

<sup>16</sup>Coyle and Siedle, p 203.

<sup>17</sup>Coyle and Siedle, p 200.

Finally, ferrous metal parts are worn to produce oxides  $\text{Fe}_2\text{O}_3$  and  $\text{Fe}_3\text{O}_4$ .<sup>18</sup>

Although specific chemical and physical forms of metals in used oil are not entirely known, filtration and centrifugation have revealed small particles of lead, zinc, calcium, barium, magnesium, and iron.<sup>19</sup> As much as 50 percent of the lead present in used crankcase oil is believed to occur as fine suspended particles.<sup>20</sup>

Water contamination occurs as a product of fuel combustion, condensation, and seepage into storage tanks.<sup>21</sup> Water contamination varying from 0.2 to 33.8 percent by volume has been reported.<sup>22</sup> An analysis of the water in a contaminated oil sample may show large amounts of sodium, zinc, barium, calcium, iron, phosphorus, magnesium, boron, tin, and lead. This implies that the metals are present in ionic or salt-like forms. Consequently, simple separation of oil and water will remove some metals.<sup>23</sup>

Generally, factors such as length of drain intervals, extent of fuel leakage into the oil, engine operating conditions, and climate influence the rates of chemical and physical reactions in the oil, and therefore dictate the oil's metal profile.<sup>24</sup>

Analysis of used oil quality is important because the cost and effectiveness of recycling processes depend on the specific chemical forms of the metals.<sup>25</sup>

#### Contamination During Handling

The most serious contamination may occur after the oil has been drained from the crankcase. During CERL's sampling exercise, nearly all maintenance unit storage tanks were found to have been used as dumpsters. Oil filters, rags, cans, trash, and water were in

these tanks. CERL also found significant concentrations of volatile liquids, probably solvents or fuels. In some tanks, up to 1 ft of water had accumulated. Any of these contaminants make the oil less valuable for reuse as re-refining stock or boiler fuel.

Table 5  
Characteristics of Used Oil

| Property or Element                                | Used Oil         |
|--|------------------|
| Viscosity (SUS* @ 40 °C)                           | 87 to 837        |
| American Petroleum Institute (API) gravity (60 °F) | 19.1 to 31.3     |
| Specific gravity                                   | 0.87 to 0.94     |
| Water (%) by volume)                               | 0.2 to 33.8      |
| BS & W** (%) by volume)                            | 0.1 to 42        |
| Benzene insolubles (%) by volume)                  | 0.56 to 3.33     |
| Gasoline (%) by volume)                            | 2.0 to 9.7       |
| Flash point (°C)                                   | 79 to 219        |
| Heating value (Btu/lb)                             | 13,570 to 19,300 |
| Ash, sulfated (%) by weight)                       | 0.03 to 6.43     |
| Carbon residue (%) by weight)                      | 1.82 to 4.43     |
| Aluminum (ppm)                                     | 0.5 to 800       |
| Barium (ppm)                                       | 9 to 3906        |
| Cadmium (ppm)                                      | 4                |
| Calcium (ppm)                                      | 211 to 3600      |
| Chromium (ppm)                                     | 8 to 50          |
| Copper (ppm)                                       | 4 to 348         |
| Iron (ppm)   | 50 to 2401       |
| Lead (ppm)   | 85 to 21,700     |
| Magnesium (ppm)                                    | 10 to 1100       |
| Phosphorus (ppm)                                   | 319 to 2000      |
| Silicon (ppm)                                      | 10 to 875        |
| Sodium (ppm)                                       | 16 to 300        |
| Sulfur (%) by weight)                              | 0.17 to 1.09     |
| Zinc (ppm)   | 260 to 3000      |

(Table derived from D. A. Becker and J. J. Comford, *Recycled Oil Program, Phase 1 Test Procedures for Recycled Oil Used as a Burner Fuel*, Technical Note 1130 [National Bureau of Standards, 1980]; T. D. Coyle and A. R. Siedle, "Metals in Oil: Occurrence and Significance for Reuse of Spent Automotive Lubricating Oils," *Proceedings of a Workshop on Measurement and Standards for Recycled Oil-II*, Gaithersburg, Maryland, National Bureau of Standards, 1977 [NBS Special Publication 556, 1979].)

\*SUS: Saybolt Universal Seconds

\*\*BS & W: bottom settlings and water

<sup>18</sup>Coyle and Siedle, p 203.

<sup>19</sup>Coyle and Siedle, p 203.

<sup>20</sup>Coyle and Siedle, p 23.

<sup>21</sup>Coyle and Siedle, p 199.

<sup>22</sup>D. A. Becker and J. J. Comford, *Recycled Oil Program, Phase 1 Test Procedures for Recycled Oil Used as a Burner Fuel*, Technical Note 1130 (National Bureau of Standards, 1980), p 5.

<sup>23</sup>Coyle and Siedle, p 207.

<sup>24</sup>Coyle and Siedle, pp 193, 199.

<sup>25</sup>Coyle and Siedle, p 199.



**Table 6**  
**Lubricating Oil Additives and Contaminants Likely To Be Found in Used Motor Oils**

(See H. A. Braier, "Metals in Oils," *Anal. Chem.*, Vol 43, No. 185R [1971], and R. F. Terrell, *Anal. Chem.*, Vol 49, No. 255R [1977]; B. R. Williams, "Automotive Crankcase Drainings Used for Fuel," *Proceedings of a Workshop on Measurements and Standards for Recycled Oil*, Gaithersburg, Maryland, National Bureau of Standards, 1976 [NBS Special Publication 488, 1977]; *Finnegan Spectra*, Vol 6, No. 2 [Sunnysale, California: Finnegan Corp., 1976].)

| Typical Additives  | Primary Source and Type of Typical Contaminants   |
|--|---|
| Antiwear: zinc organo-dithiophosphates, organic phosphorus compounds.  | Gasoline: lead and lead compounds, halogens.  |
| Corrosion inhibitors: sulfonates, amine phosphates, organic phosphites.  | Additives: zinc and zinc compounds, phosphorus compounds, etc.                            |
| Detergents and dispersants: calcium, magnesium, barium, and zinc sulfonates, phosphonates, and phenates; alkenyl succinimides; acrylic polymers. | Combustion products: polynuclear aromatics, water, oxygenated compounds, sludge, varnish. |
| Viscosity index improvers: isobutylene polymers, acrylate polymers.  | Fuel: volatile liquid.  |
| Pour-point depressants: polymethacrylates, polyacrylamides.  | Contamination: dirt, wear metals.   |
| Antifoam agents: silicones, synthetic polymers.  | Coolant leaks: water, ethylene glycol.  |
| Antioxidants: zinc organo-dithiophosphates, hindered phenols, aromatic amines, sulfurized phenols.   |   |

The solid trash problem could be corrected easily by putting screens over the inlet holes of the tanks. There would be fewer problems with water in the tanks if installations put spring closures on the tank lids and trained the troops in proper disposal methods. In addition, Fort Eustis personnel suggested putting the maintenance storage tanks on the outside of the compound enclosure. This would allow easy access for the contractor collecting the oil; additional piping would permit the tanks to be filled from inside the compound.

#### **Is Army Waste Oil a Hazardous Waste?**

A material is considered a hazardous waste if: (1) it is ignitable, corrosive, reactive, or toxic as defined in subpart c of 40 CFR Part 261, or (2) it is listed in subpart d of 40 CFR Part 261, the Hazardous Waste Regulations. A facility emitting over 1000 kg per month of hazardous waste is responsible for storing, transporting, and disposing of the waste according to the regulations in 40 CFR Parts 260-265.

Waste oil has not been officially listed as a hazardous waste in the Hazardous Waste Regulations. However,

according to an EPA report, "...the following waste oils are hazardous wastes, and thus should be subject to the regulations prescribed under Sections 3002 through 3004 of RCRA: (1) Oil spilled to land, and oily debris generated from cleaning up spills to land or surface water; (2) used automotive oils; and, (3) used industrial oils." As to whether the Army's oil is "waste" or "used" oil, the EPA report states: "Used oil becomes a waste oil when it is contaminated with physical or chemical impurities resulting from use, such that the oil cannot be reused for its original purpose without first removing these impurities."<sup>26</sup> This definition suggests that oil becomes a waste when it is removed from the crankcase. In FY82, the EPA is scheduled to issue regulations dealing specifically with waste oil.

CERL's analyses of waste oil storage tank samples revealed that oil should be considered a hazardous

<sup>26</sup>Report to Congress, *Listing of Waste Oil as a Hazardous Waste Pursuant to Section (8)(2), Public Law 96-463* (EPA, January 1981).

**Table 7**  
**CERL Army Waste Oil Analysis**

|  | <b>Fort Benning</b>     |                          |                       | <b>Fort Bragg</b>       |                          |                       | <b>Fort Eustis</b>      |                          |
|--|-------------------------|--------------------------|-----------------------|-------------------------|--------------------------|-----------------------|-------------------------|--------------------------|
|  | <b>Upper<br/>Sample</b> | <b>Middle<br/>Sample</b> | <b>Top<br/>Sample</b> | <b>Upper<br/>Sample</b> | <b>Middle<br/>Sample</b> | <b>Top<br/>Sample</b> | <b>Upper<br/>Sample</b> | <b>Middle<br/>Sample</b> |
| Density (g/cc)                             | 0.903                   | 0.902                    | 0.911                 | 0.910                   | 0.912                    | 0.912                 | 0.907                   | 0.985                    |
| Specific gravity                           | 0.890                   | 0.884                    | 0.895                 | 0.892                   | 0.892                    | 0.892                 | 0.901                   | 0.989                    |
| Sulfur (%)                                 | 0.61                    | 0.71                     | 0.30                  | 0.33                    | 0.33                     | 0.71                  | 0.83                    | 0.31                     |
| Heating value                              |                         |                          |                       |                         |                          |                       |                         |                          |
| Btu/lb                                     | 19,000                  | 19,000                   | 15,700                | 15,100                  | 16,100                   | 18,700                | 18,800                  | 7,800                    |
| Btu/gal                                    | 143,000                 | 143,000                  | 119,000               | 115,000                 | 122,000                  | 142,000               | 142,000                 | 64,000                   |
| Bottom solids &<br>Water (%)               | 0.41                    | 0.50                     | 2.0                   | 6.6                     | 7.6                      | 0.2                   | 0.2                     | 6.5                      |
| Flash point (°C)                           | 85                      | 80                       | 50                    | 42                      | 46                       | 52                    | 41                      | 46                       |
| Viscosity (100° F)<br>(cSt)                | 298                     | 102                      | 16                    | 217                     | 255                      | 227                   | 219                     | 812                      |
| Lead (ppm)                                 | 480                     | 310                      | 10                    | 70                      | 220                      | 80                    | 80                      | 20                       |
| Ash (%)                                    | 1.40                    | 2.05                     | 0.29                  | 0.12                    | 0.17                     | 3.66                  | 3.77                    | 3.16                     |
| Polychlorinated<br>biphenyl (PCB)<br>(ppm) | <1.0                    | <1.0                     | <1.0                  | <1.0                    | <1.0                     | <1.0                  | <1.0                    | <1.0                     |

waste regardless of the new regulations. The ignitibility test for a hazardous waste is defined in 40 CFR Part 261.21. If a liquid has a flash point of less than 140°F (60°C), then it is ignitable and is a hazardous waste. All samples tested from Forts Bragg and Eustis, and at least one sample from Fort Benning, had flash points below 140°F. This test probably shows the presence of solvents or fuels. Improved management by segregating waste oils from other liquid wastes should alleviate problems with ignitibility.

Even if Army waste oil were classified a hazardous waste, it is not subject to the notification requirements of RCRA. Part 261.6 of the Hazardous Waste Regulations exempts wastes that are "being beneficially used or reused or legitimately recycled or reclaimed" from regulation under Parts 262 through 265, and from the notification requirements of Section 3010 of RCRA. However, this means that installations must be careful that all used oil is reused and none is disposed in another manner.

## 4 REUSE OPTIONS

### Current Policy

The 4 June 1979 memorandum from the Assistant Secretary of Defense (Manpower, Reserve Affairs, and Logistics) limits the options for disposing of used lubricating oil. The memorandum directs Defense agencies to sell as much oil as possible through DPDOs to re-refiners, and to burn the used oil as a fuel when re-refining is not economical. Disposal practices such as using the oil for weed, insect, and dust control, burning it in open pits, and dumping it into landfills or sewers are rejected as environmentally unacceptable.<sup>27</sup>

A GAO report to Congress recommends another option for recycling DOD's used oil. This report

<sup>27</sup>"Oil Recycling and Reuse Policy." Memorandum for the Secretaries of the Military Departments, the Directors Defense Agencies (Assistant Secretary of Defense [Manpower, Reserve Affairs, and Logistics], June 4, 1979).

proposes a "closed cycle" system in which a major Army installation provides used oil as a feed stock for a re-refiner and then buys back the processed oil.<sup>28</sup> The 12 January 1981 memorandum from the Assistant Secretary of Defense (Manpower, Reserve Affairs, and Logistics) endorses this option.<sup>29</sup>

#### Re-Refining

Re-refineries buy bulk quantities of used oil at a wide range of prices, depending on factors such as the quality of the used oil, competition, and so on. Used oil is often brought to these companies by independent haulers who act as middlemen between the waste oil generator and the processors. Most Army installations are now selling their oil to these independent haulers. The amount paid to the installation varies across the country, ranging from less than \$.10 per gallon to more than \$.30 per gallon. After the waste oil has been reprocessed, it is sold as lubricating oil at \$1.50 to \$2.00 per gallon. Appendix A briefly describes various re-refining processes, and Appendix B lists reprocessing companies.

#### Used Oil as a Fuel

When economically feasible, used oil may be burned as a boiler fuel. Of course the costs of using this option for disposal depend on the boiler fuel system currently used at the installation.

The three facilities CERL visited during the sampling survey were all using waste oil as a boiler fuel. As with these three boilers, conversion to waste oil burning is much more feasible if a liquid fuel system is already in use. Figure 1 is an example of a design for adding waste oil as a supplemental boiler fuel.

Impurities usually have to be pretreated before waste oil can be used as a fuel; the design in Figure 1 includes screens and filters. A system for eliminating and treating wastewater must also be provided. Suspended metals and other contaminants may cause air pollution problems. As Table 8 indicates, the Army's waste oil ranges from safe in all categories to unusable without air pollution controls on the

boilers. Air pollution problems probably would result from particulate levels and lead emissions.

Table 8 lists EPA-recommended limits on the characteristics of waste oil used as a fuel. Appendix C is a detailed assessment of waste oil as a boiler fuel.

#### Closed Loop Recycling

The closed loop system is the most promising option for reusing waste oil. The Army is not now using this method, but the railroad and auto industries are having success with it, and it was used by the military during World War II. Closed loop recycling was not possible before January 1980 because MIL-L-46152, for administrative service vehicles, and MIL-L-2104, for tactical vehicles, did not allow used oils as a feed stock. However, the administrative vehicle specification has been amended (MIL-L-46152B), and the tactical vehicle specification will be amended by mid-1982 to allow used oil as feed stock. This change, along with the memoranda mentioned earlier, permits closed loop re-refining. All re-refiners contacted by CERL have stated that they are interested in closed loop agreements.

The major obstacle to the Army's using closed loop agreements extensively is the cost of qualifying an oil to meet MIL-L-46152 requirements. For a re-refiner's product to qualify under MIL-L-46152B, it must pass expensive engine sequence tests. Re-refiners have stated that the \$50,000 cost of the engine test has kept them from trying to qualify their oil. However, they said they would be interested if the cost of testing could be included in the closed loop agreement.

#### Economic Comparison

To determine which disposal method to use, the waste oil manager must assess the costs and benefits of each. The manager should consider several factors, which vary from installation to installation: current waste oil management, availability of large storage facilities, present boiler fuel system, proximity of re-refiners, and waste oil transportation costs. A manager would probably use the following method to analyze the options.

##### 1. Selling oil to private collector.

$\$Return = \text{no. of gal of waste oil} \times \$/\text{gal (going rate paid by collector)}$

##### 2. Using oil as a boiler fuel.

$\$Return = (\$ \text{ value of replaced fuel}) - (\$ \text{ cost of handling, storage, filtering, and piping facility})$

<sup>28</sup>Ways the Department of Defense Can Improve Oil Recycling (General Accounting Office, Report to Congress, September 28, 1977).

<sup>29</sup>"Defense Environmental Actions for 1981," Defense Environmental Quality Program Policy Memorandum No. 81-1 (Assistant Secretary of Defense [Manpower, Reserve Affairs, and Logistics], 12 January 1981).

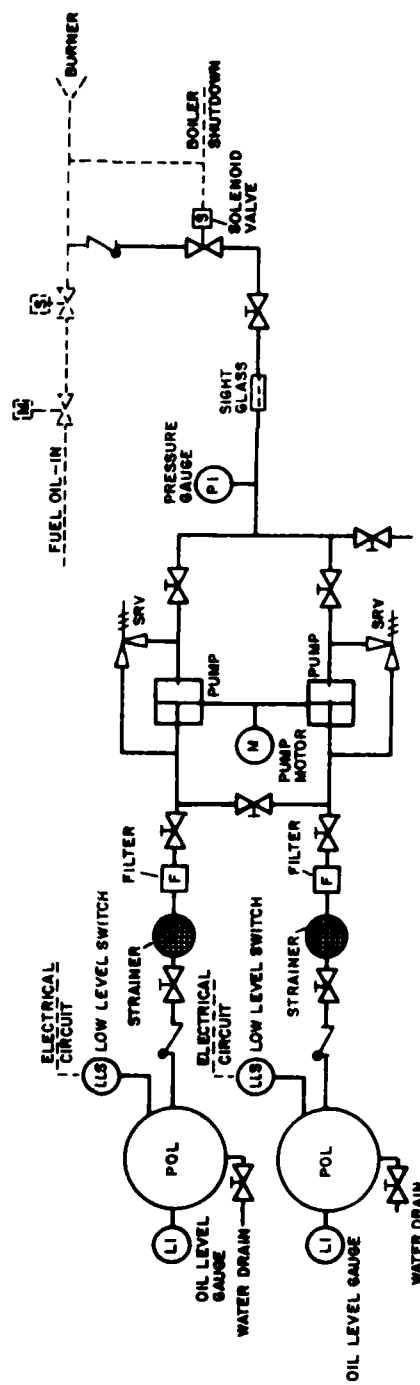


Figure 1. Conceptual flow system scheme for waste oil disposal system. (From P. L. Fink and J. W. Jackson. *Waste POL Disposal Through Energy Recovery*. [Air Force Civil Engineering Center, June 1976].)

**Table 8**  
**Characteristics of a Used Oil Which May Be Combusted**  
**With Little or No Environmental Risk**

| Characteristic*  | Comment*  | CERL Analysis<br>of Army Waste Oil |
|--|---|------------------------------------|
| Total ash $\leq$ 0.37 (by weight)                          | Equivalent to 0.12 grams/SCF emission (0% excess air).<br>Meets many state and local regs when burning 100% used oil. | 0.12 to 3.77                       |
| Lead content $\leq$ 50 ppm                                 | Meets almost all local ambient air quality standards when burning 100% used oil.                                      | 10 to 480 ppm                      |
| Chlorine $\leq$ 0.4/(weight)                               | Normal for used oils indicating no contamination by chlorinated solvents.   | Not analyzed                       |
| PCB $\leq$ 50 ppm  | Consistent with PCB criteria, 40 CFR Part 761.  | Less than 1.0 ppm                  |
| BS&W $\leq$ 1%   | Indicator absence of substantial water and sediment which may contribute to emission or burning problems.             | 0.2 to 7.6                         |
| Flash point $\geq$ 140°F (60°C)                            | Corresponding to hazardous waste classification under RCRA.   | 41 to 85°C                         |
| Sulfur: $\leq$ 0.2% (by weight)<br>$\leq$ 0.5% (by weight) | Probably meets all State regs.<br>Probably meets most State regs.   | 0.3 to 0.8%                        |

\*From *Used Oil Burned as a Fuel*, Vol 1, SW 892 (EPA, 1980), pp 1-7, 1-8.

### 3. Entering into a closed loop purchase agreement.

$\$Return = (\$value\ of\ replaced\ new\ lubricating\ oil) - (\$cost\ of\ closed\ loop\ agreement,\ transportation\ to\ and\ from\ re-refining,\ and\ cost\ of\ re-refining\ oil).$

Perhaps the best way to compare alternatives is to assume a hypothetical situation. Suppose an installation produces 100,000 gal of used oil per year. Assume major contamination has been eliminated by good management, and all of the oil can be shipped to a vacuum distillation re-refiner. Also assume that all maintenance units have storage tanks accessible to a contractor, and that administrative contracting costs are the same for all three options. All dollar figures are approximate norms derived from reported actual expenses.

### 1. Sold to private collector.

a. Costs: none.

b. Savings =  $\$.15/\text{gal} \times 100,000\ \text{gal} = \$15,000\ \text{year}$

Net Value =  $\$.15/\text{gal}$ .

### 2. Used as a boiler fuel.

a. Costs: Retrofit at boiler and oil storage (assume 20-yr life) =  $\$75,000 (\$3750/\text{yr})$ .

Cost to transfer oil to boiler storage =  
 $\$.10/\text{gal} \times 100,000\ \text{gal} = \$10,000/\text{yr}.$

Total costs =  $\$13,750/\text{yr}.$

b. Savings: 100,000 gal of used oil will replace about 85,000 gal of No. 4 fuel oil, due to differences in heating value.

$$85,000 \text{ gal} \times \$90/\text{gal} = \$76,500/\text{yr.}$$

$$\text{Net Value} = 76,500 - 13,750 = \$62,750/\text{yr.} = \$63/\text{gal.}$$

### 3. Closed loop.

Assume: 80 percent of volume is returned as new oil; re-refinery is 200 mi from installation.

a. Costs for transportation:

$$\begin{aligned} \frac{100,000 \text{ gal waste oil}}{6300 \text{ gal trip}} &= 16 \text{ trips;} \\ 16 \text{ trips} \times \frac{200 \text{ mi}}{\text{trip}} \times \frac{\$1.20}{\text{mi}} &= \$3840. \\ \frac{80,000 \text{ gal re-refined oil}}{6300 \text{ gal trip}} &= 13 \text{ trips;} \\ 13 \text{ trips} \times \frac{200 \text{ mi}}{\text{trip}} \times \frac{\$1.20}{\text{mi}} &= \$3120. \end{aligned}$$

$$\text{Transportation cost} = \$6960.$$

$$\text{b. Savings} = (80,000 \text{ gal} \times \$3.10 \text{ gal for new oil purchase}) - (80,000 \times \$1.60/\text{gal fee for re-refining service}) = \$120,000/\text{yr.}$$

$$\text{c. Net Value: } \$120,000 - 7,000 = \$113,000/\text{year} = \$113/\text{gal.}$$

The above costs are for approximate comparison only and do not reflect all costs associated with the management of waste oil. The following expenses also should be accounted for: administrative costs of contracting, pretreatment costs of the waste oil to remove water and sludge, disposal costs for the water and sludge, possible increased maintenance at the boiler facility, and improvements to the present storage and collection facilities.

### Pretreatment

The three installations CERL visited use pretreatment for their waste oil boiler fuel. All are similar to the system shown in Figure 1, but one important difference is that the installations have their two storage tanks in series, rather than in parallel, as shown in the figure. Oil is drawn from the upper

part of the first tank and pumped into the second tank. This allows much of the water and heavy sediment to settle in the bottom of the first tank, where it can be drained off periodically. The characteristics of this water and sediment have not been determined; the pollution potential should be analyzed.

Interviews with boiler operators indicate that water contamination may be beneficial. The operators say that oil containing as much as 10 percent water will burn successfully in the boilers, and that water acts as a steam cleaner and may actually decrease maintenance on the inside of the boiler. Water's effect on combustion efficiency (zero BTU's/lb) and the quality of the stack emissions is not known, and should be determined.

Pretreating oil sold to re-refiners does not seem to be common, though it may be to the Army's advantage. Sludge and particulates in the feed oil to acid-clay re-refining increase the volume of waste sludges from the process, and thereby decrease the volume of the product oil. Though the contaminants may have less effect on vacuum distillation, the process' costs still must increase.

Pretreatment could be most important for closed loop recycle agreements. By decreasing the cost of re-refining by using pretreatment, the finished oil's cost to the Army will be lower. The best pre-treatment process still needs to be determined.

### Environmental Considerations

The Army's first priority for improving waste oil management would probably be to remove solvents, waste fuels and sludges from the used oil. This should eliminate two immediate problems: handling the used oil as a hazardous waste and gaining approval of Army boilers as hazardous waste disposal facilities. However, solvents and sludges would then have to be dealt with. The most effective techniques for properly disposing of or reusing these wastes need to be determined.

In addition, waste oil managers should ensure the proper disposal of solid and liquid wastes coming from the pretreatment of the waste oil. The sediment and water drained from the bottom of storage tanks and filtration units contain emulsified oil and metals in solution or in suspension. To prevent these from entering groundwater or surface water, the wastewater should be collected and drained to a sanitary sewer, or preferably to an oil-water separation unit

preceding the sanitary sewer. A characterization study should be done on this waste stream to determine to what extent it is a pollution hazard.

As mentioned previously, burning waste oil may cause air pollution problems if ambient air standards for lead or particulates are violated. The source of lead in waste oil is undoubtedly leaded gasoline, because new oil contains no lead additives. If waste oil is burned as a boiler fuel and lead becomes an air pollution problem, then the installation should consider restricting or prohibiting the use of leaded fuels in vehicles. Filtration alone may lower particulate levels enough. Pretreatment studies need to be done to decide how to make Army oil safe for use as a boiler fuel.

The problem of waste oil spillage can be addressed immediately. Oil is often spilled while being transferred from crankcase to storage tank or from storage tank to transporting vehicle. This oil is then washed away by storm water and may contaminate surface or ground-water supplies. To prevent this, storage tanks should be placed on a smooth, impervious surface with berming to contain spills and to allow drainage through an oil-water separator to a sanitary sewer.

## 5 CONCLUSIONS AND RECOMMENDATIONS

This report has evaluated the economic and environmental aspects of used oil management, emphasizing waste oil reuse. It is concluded that:

1. Closed loop agreements to re-refine the Army's waste oil appear to be the most economical option for disposal. However, the cost to qualify re-refined oil under MIL-L-46152B prevents most re-refiners from entering into these agreements. When deciding whether a closed loop purchase agreement with a re-refiner is practical, Army installations should consider including the cost of qualifying the oil for the military specification in the total cost of the contract.

2. Using waste oil as a boiler fuel is also a disposal option, but may cause air pollution problems because of contaminants in the oil. The effects of these contaminants on ambient air quality should be quantified to determine the usefulness of waste oil for boiler fuel.

3. Contaminants, especially trash, solvents, and water, in the Army's waste oil can decrease its value for re-refining and for burning. Pretreatment of the oil may be required. The effect of such contaminants on the value of oil should be quantified.

4. Volatile organics found in samples of Army waste oil make this product a hazardous waste under the flammability criteria of the Hazardous Waste Regulations. The most likely source of this contamination is the dumping of waste solvents and fuels into waste oil storage tanks. Collection and storage should be managed so that used oil is not contaminated with solvents or fuels.

5. Water and solids drained from the bottom of waste oil storage tanks sometimes are allowed to run onto the ground and may pollute surface water and groundwater. Water and solids should be analyzed to determine their pollution potential. Wastewater should be collected and drained to a sanitary sewer.

6. Oil is frequently spilled on and around waste oil storage tanks. This oil could be carried away by storm water run-off and cause a pollution problem. Storage tanks should be placed on or buried under a non-absorbing surface with berming to contain oil spillage and direct run-off through an oil-water separator to a sanitary sewer.

7. Waste oil storage tanks at maintenance units are not always accessible to contract collectors, nor are they designed to prevent trash from being deposited in the tanks. Where possible, storage tanks should be placed outside maintenance unit compounds, with the tank inlet inside the compound. The inlets should have screening to keep trash out of the tanks.

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## APPENDIX A: RE-REFINING PROCESSES

### Acid-Clay

Acid-clay is probably the most common re-refining process in the United States (Figure A1). A pretreatment step to remove debris and water usually precedes the process. After passing through grids and screens, free water is allowed to settle. The oil is then dehydrated at 300°F and atmospheric pressure. Before going to acid treatment, the oil is cooled to 100°F over 2 days.

The acid treatment is performed with 92 percent sulfuric acid in volumes of 4 to 6 percent of the reactor volume. The coagulation reaction occurs in 24 to 48 hours. The acid sludge which contains the contaminants and ash from the oil is drawn off and disposed of.

The clay treatment removes light fuel fractions, mercaptans, and color bodies from the oil. The process occurs at 500 to 600°F and takes 15 to 16 hours. The clay itself consists of activated clay and diatomaceous earth (200 to 250 mesh). About 0.4 lb of clay is required per gallon of oil.

The final step is a filtering process. The oil passes through a filter press at 250 to 300°F. It may be filtered more than once to achieve a desired quality. The finished oil is sent to storage, where additives may be introduced.<sup>30</sup>

A typical acid-clay process yields 45 to 75 percent of the feed oil, depending largely on operating conditions and feed composition. The product of an acid-clay process is a solvent neutral blending stock with a viscosity (Saybolt Universal Seconds [SUS], 210°F) of 55 to 58 seconds, corresponding to a Society of Automotive Engineers (SAE) 20-weight oil.<sup>31</sup> Diesel crankcase drainings as feed stock produce a heavier SAE 40-weight oil with a viscosity (SUS, 210°F) of 80 to 85 seconds.<sup>32</sup>

<sup>30</sup>Waste Oil Study: A Report to the Congress, PB257693 (EPA, April 1974), pp 35-37.

<sup>31</sup>Waste Oil Study, p 40.

<sup>32</sup>G. J. Mascetti and H. M. White, *Utilization of Used Oils*, Final Report, U.S. Department of Energy Contract EY-76-C-03-1101-003/ATR7873841 (August 1978).

The major disadvantage of the process is disposing of the large volumes of acid sludge it generates. This sludge is produced at a volumetric rate of 1/10 of the oil feed rate, at least 1/10 of the incoming oil itself is contained in the sludge. Specifically, the sludge contains sulfuric acid, combustibles, lead, organometallics, sulfonates, and possibly some carcinogenic materials.<sup>33</sup> The fact that 30 to 50 percent of the sludge is soluble complicates the disposal dilemma. The sludge is combustible, but should not be burned because of the high concentration of sulfur oxides and very fine metal-containing particulates present.<sup>34</sup>

The spent clay is composed of polar compounds such as oxygen- and nitrogen-containing organics. The oil content is approximately 20 to 30 percent. Generally, the spent clay is not a disposal problem.<sup>35</sup>

### Vacuum Distillation

Vacuum distillation presents no serious disposal problem (Figure A2). The process consists of three steps: pretreatment, distillation, and finishing. The pretreatment is a dehydration step. The oil is heated to 300°F at atmospheric pressure. The overhead is sent to a decantation process and the bottoms are mixed with caustic and naptha to break up oil-water emulsions and precipitate solids.

The distillation occurs at 700 F (371°C) with a vacuum of 27 in. of Hg (686 mm of Hg). The overhead goes to the plant fuel. The bottom may have an ash content as high as 10 to 25 percent, depending on the extent of pretreatment and feed stock characteristics. The bottoms are also higher in sulfur, nitrogen, oxygen, and acidity than the feed stock. Finally, lead is concentrated in the bottoms, which may have a lead content of 5 to 15 percent.<sup>36</sup> The middle cut, or lube distillate, is sent to a finishing process (caustic clay treatment or hydrotreatment) and sold as lube oil. The properties of oil processed by vacuum distillation are listed in Table A1.

The distillation process is advantageous because more than one cut may be taken off the middle of the tower to produce several products with different viscosities. One can expect a 70 percent yield from a

<sup>33</sup>Waste Oil Study, p 44.

<sup>34</sup>Waste Oil Study, pp 44-45.

<sup>35</sup>Waste Oil Study, p 45.

<sup>36</sup>Waste Oil Study, p 46.

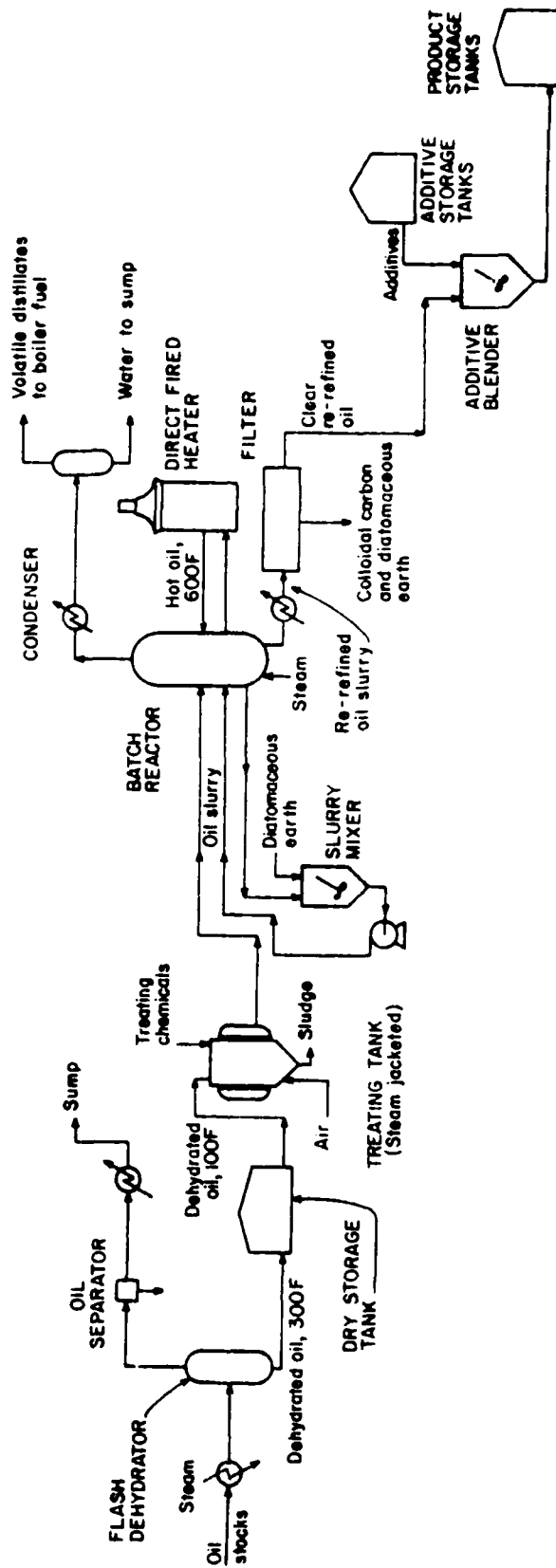


Figure A1. Acid-clay process. (From *A Technical and Economic Study of Waste Oil Recovery, Part III: Economic, Technical and Institutional Barriers to Waste Oil Recovery*, PB23760 [EPA, October 1973].)

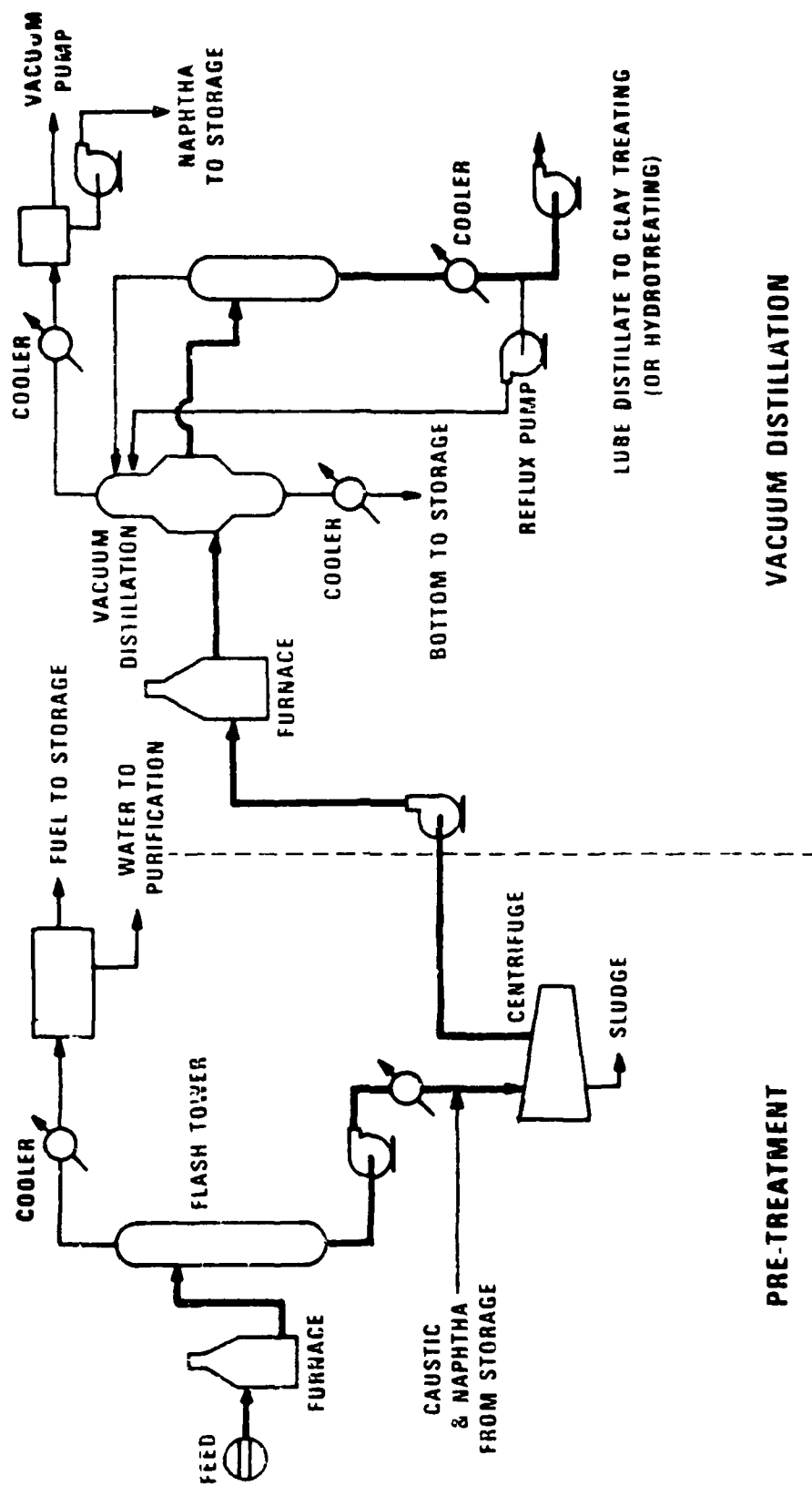


Figure A2. Vacuum distillation of crankcase waste oil. (From Waste Oil Study: A Report to the Congress, PB257693 [EPA, April 1974].)

**Table A1**  
**Properties of Used Lubricating Oil Processed by Vacuum Distillation**  
 (From M. L. Whisman, J. W. Goetzinger, and F. O. Cotton, *Waste Lubricating Oil Research*  
*Some Innovative Approaches to Reclaiming Used Oil*, U.S. Bureau of Mines, 1974, p. 17)

| Property                        | New Oil     | Used Oil   | Processed Oil | Reformulated Oil | Property                     | Hydrocarbon Analysis | Processed Oil |
|---------------------------------|-------------|------------|---------------|------------------|------------------------------|----------------------|---------------|
| Sp. gr. 60/60 I                 | 0.878       | 0.897      | 0.869         | 0.881            | Recovery, percent            | 100                  | 99            |
| Viscosity                       |             |            |               |                  | Paraffins                    |                      |               |
| SUS, 100 I                      | 280         | 265        | 149           | 265              | Recovered oil basis, percent | 80.3                 | 80.0          |
| SUS, 210 I                      | 61.2        | 58.0       | 42.9          | 54.6             | Difference, percent          | 0                    | 0             |
| CCS*                            | 16.2        | NA**       | 12.8          | 20.2             | Original oil basis, percent  | 0                    | 0             |
| Viscosity index                 | 178         | 165        | 90            | 137              | Percent                      | 50.3                 | 80.0          |
| Carbon residue                  | 1.1         | 4.3        | 0             | 1.1              | Difference, percent          | 0                    | 0             |
| Sulfated ash                    | 1.13        | 2.82       | nil           | 1.28             | Monoaromatics                |                      |               |
| Flash point, °F                 | 355         | 220        | 375           | 365              | Recovered oil basis, percent | 12                   | 11.4          |
| Pour point, °F                  | 35          | 35         | NA**          | NA               | Percent                      | 0                    | 5.79          |
| Nitrogen, percent               | 0.021       | 0.091      | 0.025         | 0.087            | Difference, percent          | 0                    | 0             |
| Sulfur, percent                 | 0.30        | 0.32       | 0.14          | 0.32             | Original oil basis, percent  | 12.1                 | 11.4          |
| Pentane insoluble               | 0.05        | 1.18       | 0.03          | 0.05             | Difference, percent          | 0                    | 5.79          |
| Antifreeze                      | NA          | neg        | NA            | NA               | Paraffinatics                |                      |               |
| Saponification No.              | 272         | 11.0       | 1.70          | 5.46             | Recovered oil basis, percent | 3.8                  | 3.8           |
| Gasoline dilution               | 0.4         | 3.0        | 0             | NA               | Percent                      | 0                    | 0             |
| Total acid No.                  | 1.27        | 4.00       | 0.251         | 2.46             | Difference, percent          | 0                    | 0             |
| Total base No.                  | 6.85        | 2.70       | 0.01          | 8.02             | Recovered oil basis, percent | 3.9                  | 4.9           |
| Falex wear                      | 17          | 102        | 63            | 42               | Difference, percent          | 0                    | 0             |
| Corrosion (seawater)            | Pass        | Pass       | Pass          | Pass             | Original oil basis, percent  | 3.8                  | 3.8           |
| Foam                            | Pass        | Pass       | NA            | NA               | Percent                      | 0                    | 0             |
| Oxidation stability:            |             |            |               |                  | Difference, percent          | 0                    | 0             |
| Appearance                      | Light brown | Dark brown | Dark brown    | Brown            | Polyaromatic and polar       |                      |               |
| Acid No. increase               | 0.12        | 0.13       | 4.48          | 0.13             | Recovered oil basis, percent | 3.9                  | 4.9           |
| Pentane insoluble increase      | 0           | 13.7       | 13.7          | 1.0              | Difference, percent          | 0                    | 0             |
| Viscosity (SUS, 100°F) increase | 0.02        | NA         | 0.05          | 0.01             | Original oil basis, percent  | 3.9                  | 4.9           |
| Metal concentration, ppm:       |             |            |               |                  | Difference, percent          | 0                    | 0             |
| Ba                              | 162         | 150        | 0             | 22               |                              |                      |               |
| Ca                              | 3,430       | 3,600      | 0             | 1,850            |                              |                      |               |
| Mg                              | 20          | 47         | 0             | 600              |                              |                      |               |
| Na                              | 5           | 18         | 0             | 5                |                              |                      |               |
| P                               | 470         | 600        | NA            | NA               |                              |                      |               |
| Zn                              | 359         | 461        | 31            | 1,248            |                              |                      |               |
| Al                              | 1           | 14         | 0             | NA               |                              |                      |               |
| Cr                              | 0           | 10         | 0             | NA               |                              |                      |               |
| Cu                              | 1           | 4          | 1             | NA               |                              |                      |               |
| Fe                              | 1           | 149        | 0             | NA               |                              |                      |               |
| K                               | 7           | 7          | 0             | NA               |                              |                      |               |
| Mn                              | 1           | 2          | 0             | NA               |                              |                      |               |
| Ni                              | 0           | 2          | 0             | NA               |                              |                      |               |
| Pb                              | 0           | 10.420     | 105           | NA               |                              |                      |               |
| Si                              | 3           | 12         | 5             | NA               |                              |                      |               |
| Sn                              | 0           | 10         | 0             | NA               |                              |                      |               |
| V                               | 0           | 0          | 0             | NA               |                              |                      |               |

\*Cold-cranking simulator (apparent viscosity)

\*\*Not available

vacuum distillation re-refining process, which is the most that can be attained with the acid clay process. The product quality is comparable to that of the acid clay process.<sup>37</sup>

#### **Solvent Extraction and Clay Treatment**

A propane extraction re-refining process is shown in Figure A3. The general treatment scheme is thermal dehydration, precipitation and solvent extraction, vacuum distillation, acid and clay treatment, and filtration.

Propane is used to selectively extract the base lube stock from additives and impurities. The propane-to-feed stock ratio must be 15 to 20:1 for a high quality product. The propane-oil mixture is removed from the extractor, and the propane is flashed from the oil and recycled. The residue at the unit bottom is a dark, asphaltic substance containing oxidized hydrocarbons and suspended solids.

The recovered lube oil next undergoes an acid-clay treatment similar to that described earlier. Because a significant amount of contamination has been removed, the acid and clay doses are only half of what would be used in an acid-clay re-refining process. The final step is filtration.<sup>38</sup>

The wastes from the process are the distillation bottoms, acid sludge, and spent clay. Even though the sludge and clay quantities are smaller than those from an acid-clay process, the disposal problem is significant because of the waste's characteristics. The color and color stability qualities of the product, however, are superior to that of an acid-clay process.<sup>39</sup>

#### **Phillips Re-Refined Oil Process**

The Phillips Petroleum Co. has developed the Phillips Re-Refined Oil Process (PROP). Phillips sells modular, skid-mounted PROP units that can treat 2, 5, and 10 million gallons per year, at costs of \$1.8, \$3.1, and \$4.3 million, respectively.

The process begins by mixing diammonium phosphate (DAP) with heated oil to remove the metals. Metallic phosphates are formed and removed by filtration. Trace inorganics are then removed by mixing the oil with hydrogen, percolating it through a bed of clay, and passing it over a nickel molybdate catalyst.

The treated oil is flashed, cooled, and put through a stripper to remove any remaining fuel.

The requirements for a 2 million gallon per year process are 900 lb/hr of 150 psi steam, 85 kW/hr of electricity, 300 gal/hr cooling water, and 0.88 million Btu/hr fuel. According to Phillips, the process recovers 90 percent of the waste oil, containing less than 10 ppm metals.

Wastes from the process include the filter cake from the demetallization, which Phillips says can be deposited in a sanitary landfill, and some wastewater, which can be sent without pretreatment into a sanitary sewer.

#### **Wastewater**

Wastewater from re-refining operations originates as water separated from new drain oil, cooling water from heat exchangers, contaminated cooling water, water from condensed steam that contacts the oil, plant runoff water, and water from vent gas scrubbers.<sup>40</sup> The water can be expected to contain some metals as dissolved or suspended solids, as well as dissolved phenols and other organics, and suspended or emulsified oil.<sup>41</sup> Wastewater characteristics depend, of course, on the re-refining process and the feed stock.

Treatment facilities required at a re-refinery depend on cooling water and vacuum facilities, water contamination of the feed stock, runoff problems, land availability, regulations, and local sewage treatment plant availability.<sup>42</sup> Typically, acid-clay and distillation-clay plants are equipped with oil-water separators and neutralization facilities.<sup>43</sup>

#### **Air Pollution**

A properly operating re-refinery emits very few air pollutants; sources of these are vents from process and wastewater treatment units, and storage tanks. Emissions may be discharged to a furnace where combustible materials are burned. Any odors from a plant are probably due to esters and other organic compounds containing oxygen and nitrogen. Very low concentrations of organic sulfur compounds may be emitted. Acid-sludge processes may produce SO<sub>2</sub> and SO<sub>3</sub>.<sup>44</sup>

<sup>37</sup>Waste Oil Study, p 37.

<sup>38</sup>Waste Oil Study, pp 40-42.

<sup>39</sup>Waste Oil Study, p 42.

<sup>40</sup>Waste Oil Study, p 46.

<sup>41</sup>Waste Oil Study, p 47.

<sup>42</sup>Waste Oil Study, p 39.

<sup>43</sup>Waste Oil Study, p 46.

<sup>44</sup>Waste Oil Study, p 47.

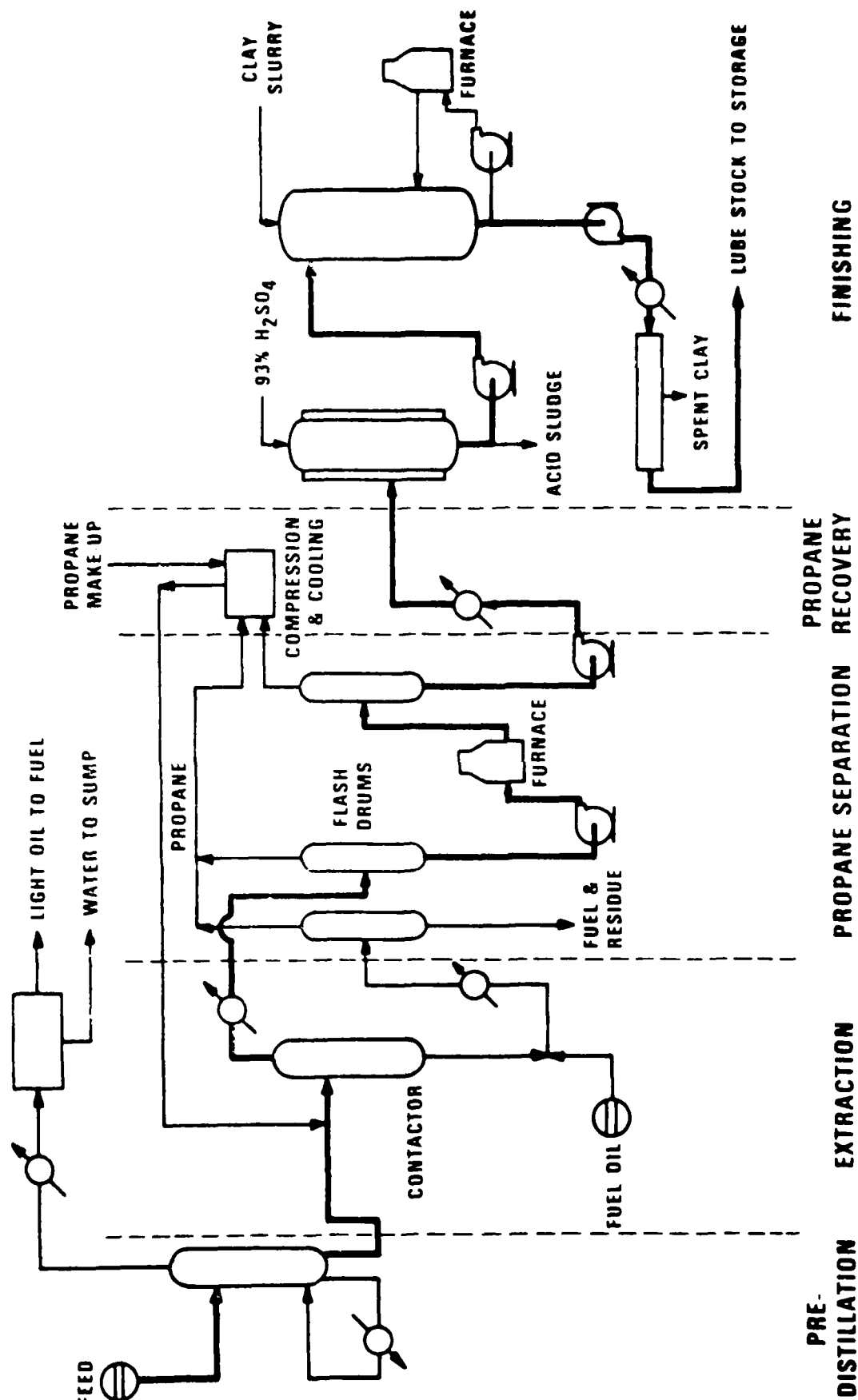


Figure A3. Refining by a propane extraction process. (From Waste Oil Study - 1 Report 1, The Company PB257693 [EPA, April 1974])

**APPENDIX B:  
WASTE OIL RE-REFINERS  
AND PROCESSORS**

**Arkansas**

Henley Oil Company  
P.O. Box 141  
Norphlet, Arkansas 71759  
Telephone: 501-546-2582  
Contact: Charles W. Henley

**California**

Bayside Oil Corporation  
977 Bransten Road  
San Carlos, California 94070  
Telephone: 415-593-2944  
Contact: A. Ray Banks

Leach Oil Company, Inc.  
625 East Compton Blvd.  
Compton, California 90220  
Telephone: 213-323-0116  
Contact: George Leach

C. S. McAuley, Inc.  
P.O. Box 219  
Downey, California 90241  
Telephone: 213-869-1179  
Contact: C. S. McAuley

Motor Guard Lubricants Co.  
4334 East Washington Blvd.  
Los Angeles, California 90023  
Telephone: 213-268-6877  
Contact: H. B. Millard

Fabian Oil Refining Co.  
4200 Alameda Avenue  
Oakland, California 94601  
Telephone: 415-532-5051  
Contact: Bryan Fabian

Talley Bros. Inc.  
2007 Laura Avenue  
Huntington Park, California 90255  
Telephone: 213-587-1217  
Contact: A. W. Talley

Nelco Oil Refining Company  
1211 McKinley Avenue  
National City, California 92050  
Telephone: 714-474-7511  
Contact: Otis F. Humphrey

**Colorado**

Williams Refining Company  
5901 North Federal St.  
Denver, Colorado 80221  
Telephone: 303-433-2497  
Contact: Lloyd Cunningham

**Florida**

Davis Oil Company  
Box 1303, 1100 Orange Ave.  
Tallahassee, Florida 32302  
Telephone: 904-576-3116  
Contact: George Davis

Peak Oil Company  
Route 3, Box 24  
Tampa, Florida 33619  
Telephone: 813-626-9116  
Contact: John Schroter

Petroleum Products Co.  
Box 336, South Park Road  
Pembroke Park  
Hallendale, Florida 33009  
Telephone: 305-989-4000  
Contact: Sol Blatt

Seaboard Oil Industries of Florida, Inc.  
Box 6336  
Jacksonville, Florida  
Telephone: 904-389-8845  
Contact: Byron Cohen

**Georgia**

Seaboard Industries  
Box 47333  
5810 New Peachtree Road  
Doraville, Georgia 30040  
Telephone: 404-458-2241  
Contact: Bryon Cohen



**Illinois**

Central Refining Company  
2000 E. Madison  
P.O. Box 3063  
Springfield, Illinois 62703  
Telephone: 217-525-2309  
Contact: Martin Pierce

Estech Oil Company  
7601 West 47th Street  
McCook, Illinois 60525  
Telephone: 312-242-2252  
Contact: John O'Connell

**Indiana**

Westville Oil & Mfg. Inc.  
Box 587, State Road #2  
Westville, Indiana 46391  
Telephone: 219-785-2534  
Contact: Andrew Carson

**Kansas**

Coral Refining Company  
765 Pawnee Avenue  
Kansas City, Kansas 66105  
Telephone: 913-281-5454  
Contact: Robert O'Blasny

Resource Technology, Inc.  
809 S. 7th Street  
P.O. Box 5187  
Kansas City, Kansas 66119  
Telephone: 913-621-0000  
Contact: Timothy F. Sparks

**Michigan**

Dearborn Refining Company  
3901 Wyoming Avenue  
Dearborn, Michigan 48120  
Telephone: 313-VI-3-1700  
Contact: Jack W. Epstein, B. Horton

**Minnesota**

Warden Oil Company  
187 Humboldt Avenue North  
Minneapolis, Minnesota 55405  
Telephone: 612-374-1200  
Contact: A. L. Warden

Gopher State Oil Co.  
2500 Delaware St., SE  
Minneapolis, Minnesota 55405  
Telephone: 612-331-5936  
Contact: C. H. Romness

**Mississippi**

Jackson Oil Products Co.  
Box 5685  
Jackson, Mississippi 39208  
Telephone: 601-939-3131  
Contact: H. K. Robertson

**Missouri**

Midwest Oil Refining Co.  
1900 Walton Road  
St. Louis, Missouri 63114  
Telephone: 314-427-2662  
Contact: Glen Gettinger

Clayton Chemical Company  
10 S. Brentwood Blvd.  
Clayton, Missouri 63105  
Telephone: 314-726-6320  
Contact: Bud Haney

**New Jersey**

Diamond Head Oil Refining Co.  
1427 Harrison TnPk.  
Kearney, New Jersey 07032  
Telephone: 201-991-5800  
Contact: Martin Morrison

National Oil Recovery Corp.  
Box 338  
Bavonne, New Jersey 07002  
Telephone: 201-437-7300  
Contact: Solfred Maizus

**New York**

George T. Booth & Son, Inc.  
76 Robinson Street  
North Tonawanda, New York 14120  
Telephone: 716-693-0861  
Contact: George T. Booth

Northeast Oil Company  
327 Edward Drive  
Fayetteville, New York

Telephone: 315-454-4180  
Contact: R. W. Mahler

Newton Refining Corp.  
3780 Review Avenue  
Long Island City, New York 11101  
Telephone: 212-RA9-7660  
Contact: R. W. Mahler

#### **North Carolina**

Seaboard Industries, Inc.  
South Oil Division  
Box 106, Old Burlington Road  
Greensboro, North Carolina 27402  
Telephone: 919-375-5811  
Contact: Byron Cohen

#### **Ohio**

Research Oil Refining Company  
3680 Valley Road  
Cleveland, Ohio 44109  
Telephone: 216-749-2777  
Contact: Jac Fallenberg, Allan Gressel

Keenan Oil Company  
#1 Parkway Drive  
Cincinnati, Ohio 45212

Telephone: 513-631-2900  
Contact: S. R. Passell

#### **Oklahoma**

Double Eagle Refining Co.  
Box 11257  
Oklahoma City, Oklahoma 73111  
Telephone: 405-232-0244  
plant: 405-232-6878  
Contact: Frank Kerran, Cameron L. Kerran

#### **Oregon**

Nu-Way Oil Company  
7039 NE 46th Avenue  
Portland, Oregon 97218  
Telephone: 503-281-9375  
Contact: A. L. Geary

Ager & Davis Refining Co.  
9901 NE 33rd Street  
Portland, Oregon 97211  
Telephone: 503-288-3584  
Contact: Harold W. Ager, Jr.

#### **Pennsylvania**

Berks Associations, Inc.  
Box 617  
Pottstown, Pennsylvania 19464  
Telephone: 215-385-3031  
Contact: Lester Schurr

Petrocan Corporation  
P.O. Box 547  
Valley Forge, Pennsylvania 19481  
Telephone: 215-383-5262  
Contact: John Cunningham

#### **Tennessee**

Gurley Oil Company  
Box 2326  
Memphis, Tennessee 38102  
Telephone: 901-527-9940  
Contact: William M. Gurley

#### **Texas**

S&R Oil Company  
Box 35516  
Houston, Texas 77035  
Telephone: 713-729-8740  
Contact: R. A. Swasey

Capital Supply & Refining Co.  
Box 597  
1401 West Hurst Blvd.  
Hurst, Texas 76053  
Contact: Abel Theriot

Texas American Oil  
300 Westwall, Suite 1012  
Midland, Texas 79701  
Telephone: 915-683-4811  
Contact: William F. Judd

#### **Utah**

Alco Refining Company  
133 North First West  
Salt Lake City, Utah 84113  
Contact: J. R. Mastelotto

Ekotek Lube, Inc.  
P.O. Box 2106  
Salt Lake City, Utah 84110  
Telephone: 801-487-5984

**Virginia**

A. C. Oil Company  
1500 North Quincey St.  
Arlington, Virginia 22207  
Contact: V. T. Worthington

**Washington**

QFD Corporation  
P.O. Box 1004  
Renton, Washington 98055

Telephone: 206-271-1540  
Contact: William S. Kemp

**Wisconsin**

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1910 South 73rd  
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## APPENDIX C: USED OIL AS A BOILER FUEL

Thousands of gallons of used crankcase oil are burned each year in Army boilers. Before an installation makes a commitment to such an oil disposal program, economic and environmental factors must be considered. Although using waste crankcase oil as a supplement or alternative to virgin fuel probably will reduce fuel costs, stack emissions of lead and other pollutants may increase significantly. The combustion performance of the boilers may be impaired. Maintenance may be needed more often because of rapid deposit buildup. Boiler parts may have to be replaced more frequently. Pretreatment of the used oil or boiler modification may eliminate some of the problems but will add to the capital expense of modifying the system. Finally, one must consider the availability (present and future) of used oil; fuel requirements, which are a function of heating season length; and current fuel prices and trends.

### Air Pollution Legislation

The Clean Air Act of 1970, with amendments in 1974 and 1977, includes regulations which may affect the burning of used oil as a virgin fuel supplement or alternative. The National Ambient Air Quality Standard (NAAQS) (40 CFR Part 50) for lead is relevant because of the significant concentration of lead in automotive crankcase drainings. The NAAQS for total suspended particles is of concern since the higher ash content of used oil contributes to higher particulate emissions. Since the sulfur content of used oil is not significantly higher than that of virgin fuel oil, the SO<sub>2</sub> emissions from a boiler using recycled fuel will not be higher. Similarly, the NO<sub>x</sub> emissions are approximately equal for recycled and virgin fuel.

Where air quality is better than the NAAQS, it is preserved by the Prevention of Significant Deterioration program. This may apply to some boilers modified to burn used oil and to some new boilers. Some modified boilers may not have to undergo the entire permit process.

The Nonattainment Provisions of NAAQS may affect new or modified sources that potentially will emit more than 100 ton/year of any regulated pollutant, or that lie in or affect a nonattainment region.

The New Source Performance Standards of NAAQS apply to new or modified generators with heat inputs

greater than  $250 \times 10^6$  Btu/hr. Army boilers, though seldom this large, may be restricted by State and local regulations.

The Toxic Substance Control Act (PL 94-469) regulates used oil burning with respect to PCBs. See 40 CFR Part 761, May 31, 1979 for the most recent PCB regulations.<sup>45</sup>

### Used Oil/Virgin Oil Blends

Generally, the values of properties of blends are linear with the proportion in each oil. The exceptions are viscosity and API gravity, important characteristics of a boiler fuel. Viscosity affects the flow rate of the fuel and the spray pattern from the nozzle.<sup>46</sup> The viscosity of a blend can be determined from a plot such as that in Figure C1. The desirable firing temperature for a given viscosity can then be obtained from Figure C1.

The API gravity of an oil (expressed as degrees API) is a function of the specific gravity and can be calculated by the following equation:

$$\text{degrees API} = \frac{141.5}{S(60^\circ\text{F})} - 131.5 \quad [\text{Eq C1}]$$

where S = specific gravity of the oil.

API gravity is also related to the heat of the burning oil. Table C1 lists densities and heats of combustion for a range of gravities. Figure C2 graphs the relationship between specific gravity, API gravity, and heating value.

### Storage Considerations

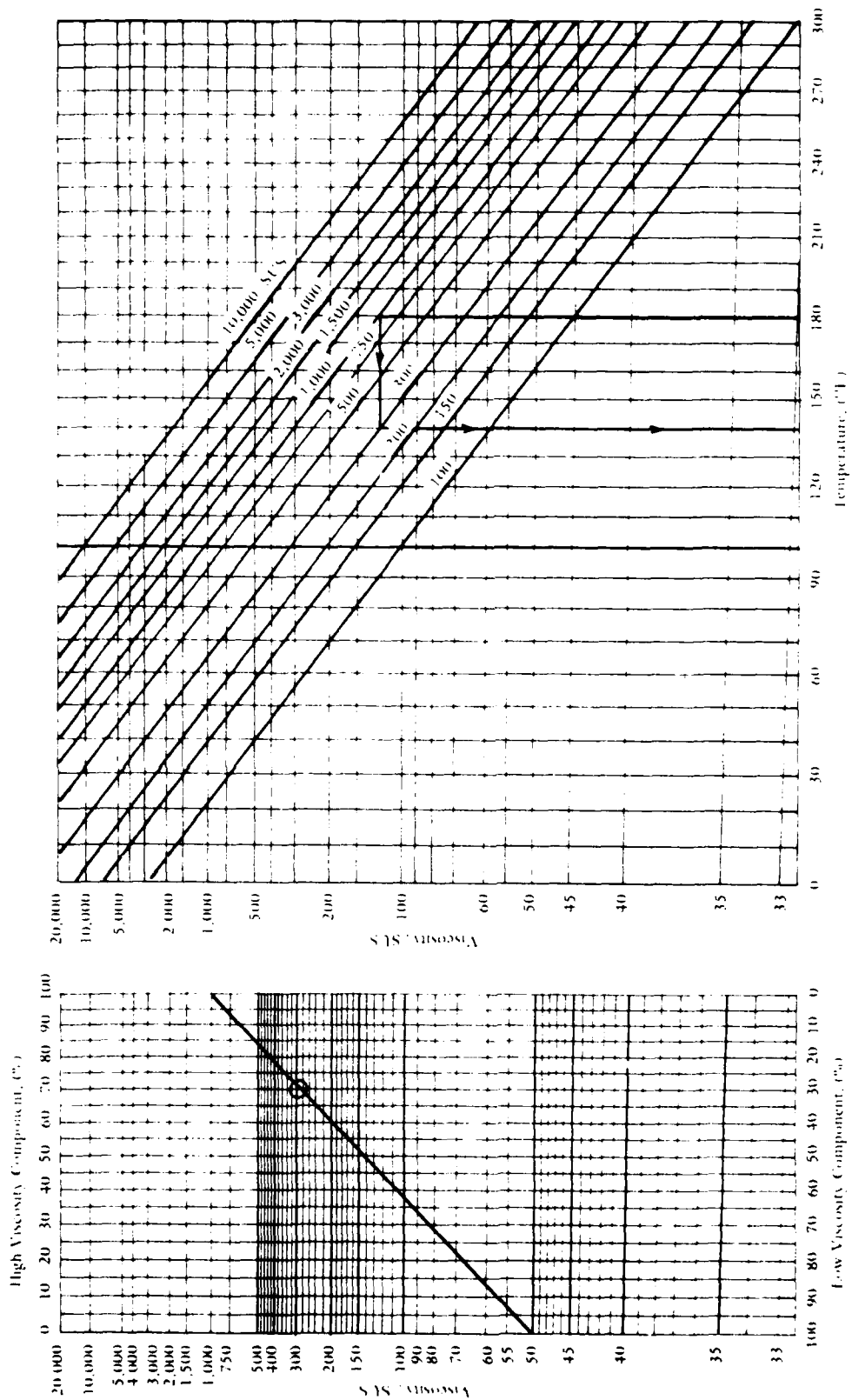
The location and design of storage facilities are affected by several safety considerations, including the proximity of heavily traveled areas and compliance with local fire codes.<sup>47</sup> Generally, storage requirements are similar to those for residual fuels.<sup>48</sup> However,

<sup>45</sup> *Used Oil Burned as a Fuel*, Vol 1, SW 892 (EPA, 1980), pp 1-6 and 1-7.

<sup>46</sup> T. T. Fu and R. S. Chapler, *Utilization of Navy-Generated Waste Oils as Boiler Fuel: Economic Analysis and Laboratory Tests*, Technical Note N-1570 (Naval Construction Battalion Center, 1980), p 14.

<sup>47</sup> P. L. Fink and J. W. Jackson, *Waste POI, Disposal Through Energy Recovery* (Air Force Civil Engineering Center, June 1976), p 5.

<sup>48</sup> G. J. Mascetti and H. M. White, *Utilization of Used Oils*, Final Report, U.S. Department of Energy Contract EY-76-C-03-1101-003/ATR7873841 (August 1978), p 10-6.

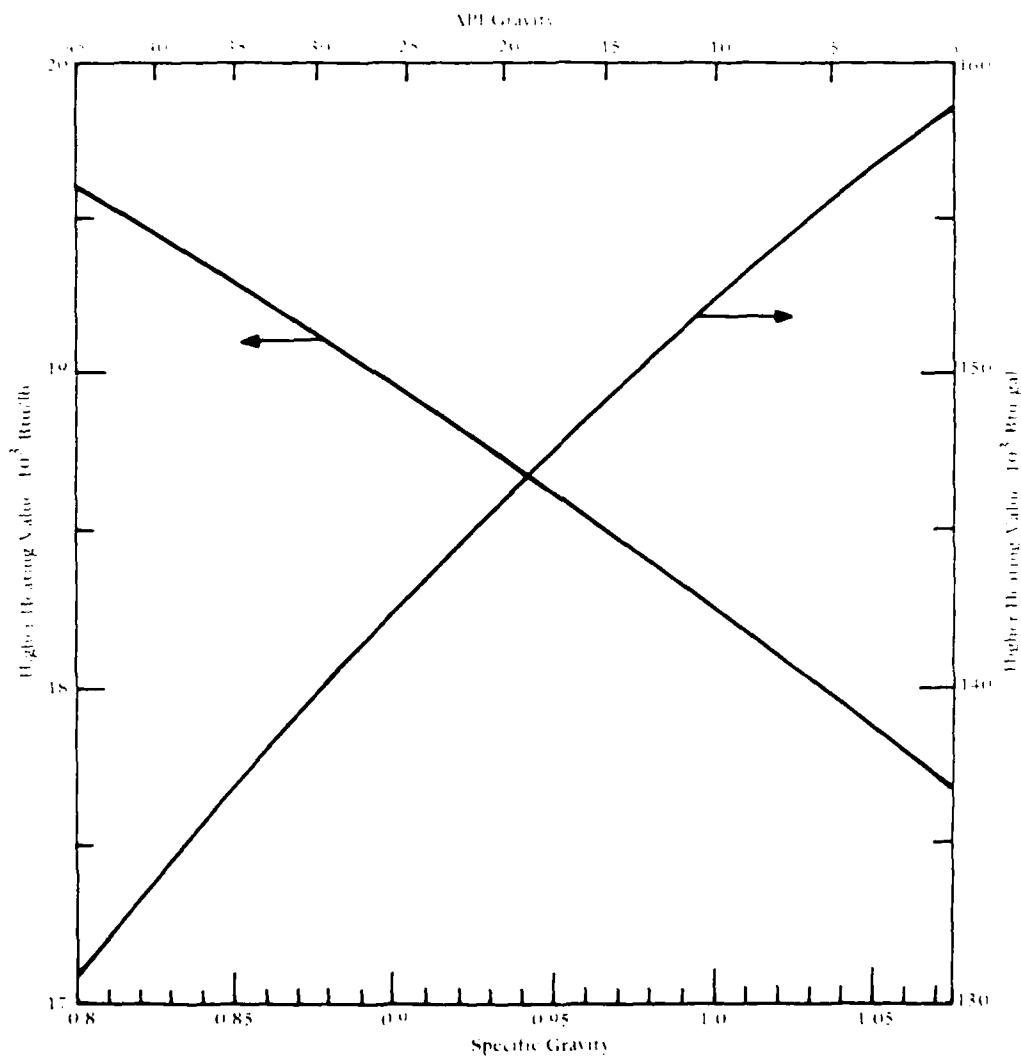


**Figure C1.** Charts for determination of firing temperatures for blending fuels. (From T. T. Fu and R. S. Chapter, *Utilization of Navy-Generated Waste Oils as Boiler Fuel - Economic Analysis and Laboratory Tests*, Technical Note N-1570 [Naval Construction Battalion Center, 1980], p. 44.)

**Table C1**  
**Gravities, Densities, and Heats of Combustion of Fuel Oils**

(From G. J. Mascetti and H. M. White, *Utilization of Used Oils*, Final Report, U.S. Department of Energy Contract EY-76-C-03-1101-003/AFR7873841 [August 1978], p. 10-3)

| GRAVITY AT 60/60 F<br>(15/15 C) |                     | DENSITY, AT<br>60 F (15 C) | TOTAL HEAT OF COMBUSTION<br>(At Constant Volume) |                                  |              | NET HEAT OF COMBUSTION<br>(At Constant Pressure) |                                  |              |
|---------------------------------|---------------------|----------------------------|--|----------------------------------|--------------|--|----------------------------------|--------------|
| DEG API                         | SPECIFIC<br>GRAVITY | LB PER<br>GAL              | BTU<br>PER LB                                    | BTU PER<br>GAL AT<br>60 F (15 C) | CAL<br>PER G | BTU<br>PER LB                                    | BTU PER<br>GAL AT<br>60 F (15 C) | CAL<br>PER G |
| 5                               | 1.0366              | 8.643                      | 18,250   | 157,700                          | 10,140       | 17,290   | 149,400                          | 9,610        |
| 6                               | 1.0291              | 8.580                      | 18,330   | 157,300                          | 10,180       | 17,340   | 148,800                          | 9,650        |
| 7                               | 1.0217              | 8.518                      | 18,390   | 156,600                          | 10,210       | 17,390   | 148,100                          | 9,670        |
| 8                               | 1.0143              | 8.457                      | 18,440   | 155,900                          | 10,240       | 17,440   | 147,500                          | 9,700        |
| 9                               | 1.0071              | 8.397                      | 18,490   | 155,300                          | 10,270       | 17,490   | 146,900                          | 9,720        |
| 10                              | 1.0000              | 8.337                      | 18,540   | 154,600                          | 10,300       | 17,540   | 146,200                          | 9,740        |
| 11                              | 0.9930              | 8.279                      | 18,590   | 153,900                          | 10,330       | 17,580   | 145,600                          | 9,770        |
| 12                              | 0.9861              | 8.221                      | 18,640   | 153,300                          | 10,360       | 17,620   | 144,900                          | 9,790        |
| 13                              | 0.9792              | 8.164                      | 18,690   | 152,600                          | 10,390       | 17,670   | 144,200                          | 9,810        |
| 14                              | 0.9725              | 8.108                      | 18,740   | 152,000                          | 10,410       | 17,710   | 143,600                          | 9,840        |
| 15                              | 0.9659              | 8.053                      | 18,790   | 151,300                          | 10,440       | 17,750   | 142,900                          | 9,860        |
| 16                              | 0.9593              | 7.998                      | 18,840   | 150,700                          | 10,470       | 17,790   | 142,300                          | 9,880        |
| 17                              | 0.9529              | 7.944                      | 18,890   | 150,000                          | 10,490       | 17,820   | 141,600                          | 9,900        |
| 18                              | 0.9465              | 7.891                      | 18,930   | 149,400                          | 10,520       | 17,860   | 140,900                          | 9,920        |
| 19                              | 0.9402              | 7.839                      | 18,980   | 148,800                          | 10,540       | 17,900   | 140,300                          | 9,940        |
| 20                              | 0.9340              | 7.787                      | 19,020   | 148,100                          | 10,570       | 17,930   | 139,600                          | 9,960        |
| 21                              | 0.9279              | 7.736                      | 19,060   | 147,500                          | 10,590       | 17,960   | 139,000                          | 9,980        |
| 22                              | 0.9218              | 7.686                      | 19,110   | 146,800                          | 10,620       | 18,000   | 138,300                          | 10,000       |
| 23                              | 0.9159              | 7.636                      | 19,150   | 146,200                          | 10,640       | 18,030   | 137,700                          | 10,020       |
| 24                              | 0.9100              | 7.587                      | 19,190   | 145,600                          | 10,660       | 18,070   | 137,100                          | 10,040       |
| 25                              | 0.9042              | 7.538                      | 19,230   | 145,000                          | 10,680       | 18,100   | 136,400                          | 10,050       |
| 26                              | 0.8984              | 7.490                      | 19,270   | 144,300                          | 10,710       | 18,130   | 135,800                          | 10,070       |
| 27                              | 0.8927              | 7.443                      | 19,310   | 143,700                          | 10,730       | 18,160   | 135,200                          | 10,090       |
| 28                              | 0.8871              | 7.396                      | 19,350   | 143,100                          | 10,750       | 18,190   | 134,600                          | 10,110       |
| 29                              | 0.8816              | 7.350                      | 19,380   | 142,500                          | 10,770       | 18,220   | 133,900                          | 10,120       |
| 30                              | 0.8762              | 7.305                      | 19,420   | 141,800                          | 10,790       | 18,250   | 133,300                          | 10,140       |
| 31                              | 0.8708              | 7.260                      | 19,450   | 141,200                          | 10,810       | 18,280   | 132,700                          | 10,150       |
| 32                              | 0.8654              | 7.215                      | 19,490   | 140,600                          | 10,830       | 18,310   | 132,100                          | 10,170       |
| 33                              | 0.8602              | 7.171                      | 19,520   | 140,000                          | 10,850       | 18,330   | 131,500                          | 10,180       |
| 34                              | 0.8550              | 7.128                      | 19,560   | 139,400                          | 10,860       | 18,360   | 130,900                          | 10,200       |
| 35                              | 0.8498              | 7.085                      | 19,590   | 138,800                          | 10,880       | 18,390   | 130,300                          | 10,210       |
| 36                              | 0.8448              | 7.043                      | 19,620   | 138,200                          | 10,900       | 18,410   | 129,700                          | 10,230       |
| 37                              | 0.8398              | 7.001                      | 19,650   | 137,600                          | 10,920       | 18,430   | 129,100                          | 10,240       |
| 38                              | 0.8348              | 6.960                      | 19,680   | 137,000                          | 10,940       | 18,460   | 128,500                          | 10,260       |
| 39                              | 0.8299              | 6.920                      | 19,720   | 136,400                          | 10,950       | 18,480   | 127,900                          | 10,270       |
| 40                              | 0.8251              | 6.879                      | 19,750   | 135,800                          | 10,970       | 18,510   | 127,300                          | 10,280       |
| 41                              | 0.8203              | 6.839                      | 19,780   | 135,200                          | 10,990       | 18,530   | 126,700                          | 10,300       |
| 42                              | 0.8155              | 6.799                      | 19,810   | 134,700                          | 11,000       | 18,560   | 126,200                          | 10,310       |
| 43                              | 0.8109              | 6.760                      | 19,830   | 134,100                          | 11,020       | 18,580   | 125,600                          | 10,320       |
| 44                              | 0.8063              | 6.722                      | 19,860   | 133,500                          | 11,030       | 18,600   | 125,000                          | 10,330       |
| 45                              | 0.8017              | 6.684                      | 19,890   | 132,900                          | 11,050       | 18,620   | 124,400                          | 10,340       |
| 46                              | 0.7972              | 6.646                      | 19,920   | 132,400                          | 11,070       | 18,640   | 123,900                          | 10,360       |
| 47                              | 0.7927              | 6.609                      | 19,940   | 131,900                          | 11,080       | 18,660   | 123,300                          | 10,370       |
| 48                              | 0.7883              | 6.572                      | 19,970   | 131,200                          | 11,100       | 18,680   | 122,800                          | 10,380       |
| 49                              | 0.7839              | 6.536                      | 20,000   | 130,700                          | 11,110       | 18,700   | 122,200                          | 10,390       |



**Figure C2.** Relationship between higher heating value and specific gravity of petroleum oils at 60°F. (From T. T. Fu and R. S. Chapler, *Utilization of Navy-Generated Waste Oils as Boiler Fuel - Economic Analysis and Laboratory Tests*, Technical Note N-1570 [Naval Construction Battalion Center, 1980], p. 39.)

contamination of the used oil with readily combustible materials such as non-halide solvents, glycols, and gasoline may raise the vapor pressure or alter the flash point of the mixture, therefore, special storage facilities may be needed.<sup>49</sup>

Drainage for gravity-settled sediment and water is an essential feature for used oil storage. Aboveground tanks should contain a drain valve, and subsurface tanks should have a suitable suction pump.<sup>50</sup> One of Fort Benning's two used oil storage tanks is shown in Figure C3.

The used oil-virgin oil blend must be mixed or agitated to prevent segregation of the oils over time because of density differences. Military Specification VV-F-815D, "Fuel Oil, Burner," requires either mechanical mixing or in-line blending of oil mixtures.

### Boilers

A major consideration is the effect of used oil combustion on the boiler itself. Of course, used oil characteristics such as water and ash content, concentrations of various additives, and the degree of dilution with virgin oil determine the quality of oil actually entering the boiler (Table C2). Short-term burning of used oil probably does not significantly affect combustion efficiency or damage boiler equipment.

Some problems can be expected, though, as a result of long-term used oil combustion: clogging of pipes and nozzles, accelerated corrosion of pipes and tanks, and reduction of heat transfer efficiency. Sediment can clog transfer piping, and water may corrode tanks and pipes, as well as freeze fuel lines.<sup>51</sup> Oil additives may cause a fine lint buildup in barrels and nozzles, ash buildup in the fire box, and deposits on boiler tubes.<sup>52</sup>

Additives are available that can help solve these problems with burning used oil.

### Emissions

Army boilers can be generally characterized as industrial-sized. That is, they have a capacity between  $50 \times 10^6$  and  $250 \times 10^6$  Btu/hr. Industrial-sized boilers usually burn residual fuel (or No. 4, 5, or 6 fuel oil) at a rate of 70 to 3500 gal/hr with 15 percent excess air.<sup>53</sup> Some are converted stoker-fired coal boilers. Others were constructed as oil-fired boilers. Few have modern air pollution control equipment. Many converted coal boilers have outdated, inefficient cyclones; some boilers have none. Oil-fired boilers usually do not have pollution control equipment. (Virgin fuel oil is a relatively clean-burning fuel.) Therefore, emissions from Army boilers burning used oil probably will be uncontrolled and should be carefully evaluated before a decision is made to fire used oil.

The number of pollutants emitted from a stack is a function of the characteristics of the oil and the combustion equipment itself. Pollutants of concern include lead and other heavy metals from the ash, sulfur, nitrogen, chlorine, and bromine originating from the ash and organic fractions. Also of concern are polynuclear aromatics (PNAs) and polycyclic organic matter (POMs) from the combustion of fossil fuels. PCBs are not normally found in used oils but if the used oil has been contaminated, burning it in an Army boiler would be not only harmful to the environment and the health of personnel, but also illegal. Other contaminants that affect emissions include gasoline, glycol antifreeze, pesticides, halides, and other solvents.<sup>54</sup>

### Lead Emissions

Lead emissions from burning used oil are a function of the firing rate (liters per hour), lead concentration of the oil, and the percent of that lead which is emitted with the flue gas. Figure C4, data collected by the EPA from 1969 to 1978, shows an inverse relationship between lead emissions and the lead concentration in the total oil (used oil and virgin fuel).

<sup>49</sup> *Used Oil Burned as a Fuel*, Vol 1, SW 892 (EPA, 1980), p 4-7.

<sup>50</sup> P. L. Fink and J. W. Jackson, *Waste POL Disposal Through Energy Recovery* (Air Force Civil Engineering Center, June 1976), p 5.

<sup>51</sup> T. D. Coyle and A. R. Siedle, "Metals in Oil: Occurrence and Significance for Reuse of Spent Automotive Lubricating Oils," *Proceedings of a Workshop on Measurements and Standards for Recycled Oil-II*, Gaithersburg, Maryland, National Bureau of Standards, 1977 (NBS Special Publication 556, 1979), p 199.

<sup>52</sup> T. T. Fu and R. S. Chapler, *Utilization of Navy-Generated Waste Oils as Boiler Fuel: Economic Analysis and Laboratory Tests*, Technical Note N-1570 (Naval Construction Battalion Center, 1980), pp 1-2.

<sup>53</sup> J. T. Beard, F. A. Lachet, and J. L. U. Lilleht, *Pollution Training Institute Course 427: Combustion Evaluation Student Manual*, EPA 450/2-80-063 (EPA, February 1980), p 8-2.

<sup>54</sup> *Used Oil Burned as a Fuel*, p 4-1.



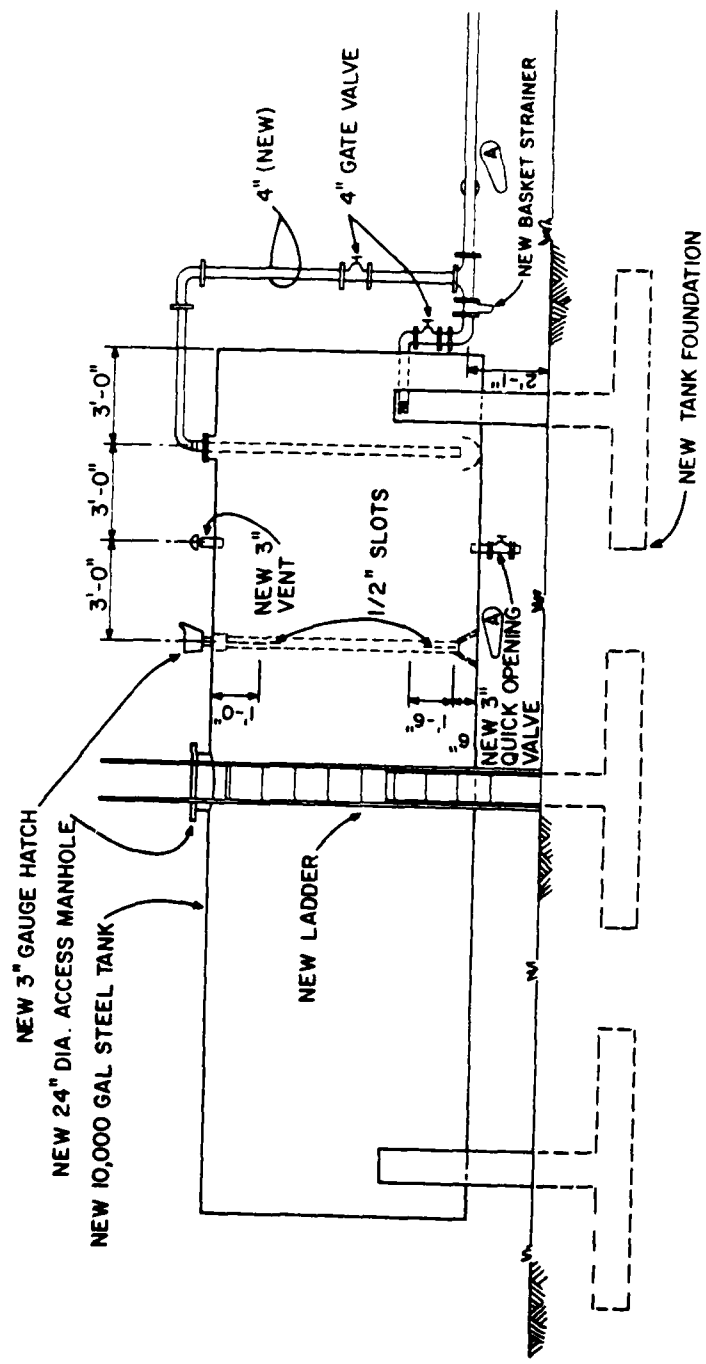


Figure C3. Storage tank at Fort Benning

**Table C2**  
**Properties of Virgin Fuel Oil (No. 2 Distillate and No. 6 Residual) and**  
**Used Oil (Automotive Crankcase Drainings)**

(From G. J. Mascetti and H. M. White, *Utilization of Used Oils*, Final Report, U.S. Department of Energy Contract EY-76-C-03-1101-003/AFR7873841 [August 1978], p. 10-4)

| Property <sup>(a)</sup>             | Composite Range Values |                       |                                    |
|-------------------------------------|------------------------|-----------------------|------------------------------------|
|                                     | No. 2 Distillate       | No. 6 Residual        | Used Oil, Crank-<br>case drainings |
| Gravity, deg API at 60°F            | 30.2 to 45.3           | 0.3 to 26.0           | 20.0 to 27.9                       |
| Specific Gravity                    | 0.800 to 0.875         | 0.898 to 1.022        | 0.887 to 0.934                     |
| Density, lb/gal                     | 6.68 to 7.30           | 7.5 to 8.5            | 7.40 to 7.78                       |
| Viscosity, SFS at 122°F             | -                      | 24 to 350             | -                                  |
| Viscosity, SUS at 100°F             | 32 to 40               | -                     | 37 to 837                          |
| Viscosity, Centistokes              | 1.8 to 4.1             | 7 to 750              | 17.3 to 180.6                      |
| Pour Point, °F                      | <-50 to 25             | <-10 to 95            | <-40 to <-30                       |
| Flash Point, °F                     | 126 to 204             | 150 to 270            | 175 to 415                         |
| Heating Value, Btu/gal              | 130,900 to 141,800     | 146,100 to (>157,700) | 105,555 to 143,360                 |
| Heating Value, Btu/lb               | 18,145 to 19,895       | 17,410 to (>20,480)   | 13,571 to 19,300                   |
| Neutralization Number,<br>mg KOH/gm | -                      | -                     | 4.0 to 14.3                        |
| Bottom Solids and Water,<br>vol %   | 0.00 to (<0.1)         | 0.00 to 2.00          | 0.1 to 22.0                        |
| Sulfur, wt %                        | 0.02 to 0.59           | 0.3 to 4.0            | 0.21 to 0.55                       |
| Ash, wt %                           | 0.00 to 0.005          | 0.00 to 0.50          | 0.03 to 3.78                       |
| Silicon, ppm                        | -                      | 8.2 to 164.0          | 10 to 875                          |
| Calcium, ppm                        | -                      | 0.7 to 95.0           | 700 to 3,000                       |
| Sodium, ppm                         | -                      | 1 to 480              | 16 to 300                          |
| Iron, ppm                           | -                      | 10.5 to 230.0         | 50 to 2,000                        |
| Magnesium, ppm                      | -                      | 0.4 to 27.9           | 10 to 1,108                        |
| Lead, ppm                           | -                      | 1.7 to 4.1            | 900 to 11,200                      |
| Vanadium, ppm                       | -                      | 1 to 380              | 3 to 39                            |
| Copper, ppm                         | -                      | 0.5                   | 5 to 348                           |
| Barium, ppm                         | -                      | -                     | 10 to 2,000                        |
| Chromium, ppm                       | -                      | 13.7                  | 3 to 50                            |
| Nickel, ppm                         | -                      | 3 to 118              | 3 to 30                            |
| Aluminum, ppm                       | -                      | 0.5 to 219            | 10 to 800                          |
| Silver, ppm                         | -                      | 0.3                   | 1                                  |
| Titanium, ppm                       | -                      | 5.5                   | 5 to 30                            |
| Molybdenum, ppm                     | -                      | 2.3                   | 2 to 3                             |
| Zinc, ppm                           | -                      | -                     | 300 to 3,000                       |
| Phosphorus, ppm                     | -                      | -                     | 500 to 2,000                       |
| Tin, ppm                            | -                      | -                     | 5 to 112                           |
| Beryllium, ppm                      | -                      | -                     | 6                                  |
| Manganese, ppm                      | -                      | -                     | 5 to 10                            |
| Cadmium, ppm                        | -                      | -                     | 4                                  |
| Strontium, ppm                      | -                      | -                     | 10 to 30                           |
| Boron, ppm                          | -                      | -                     | 3 to 20                            |

<sup>(a)</sup> ppm (as the element) = 0.0001 wt %.

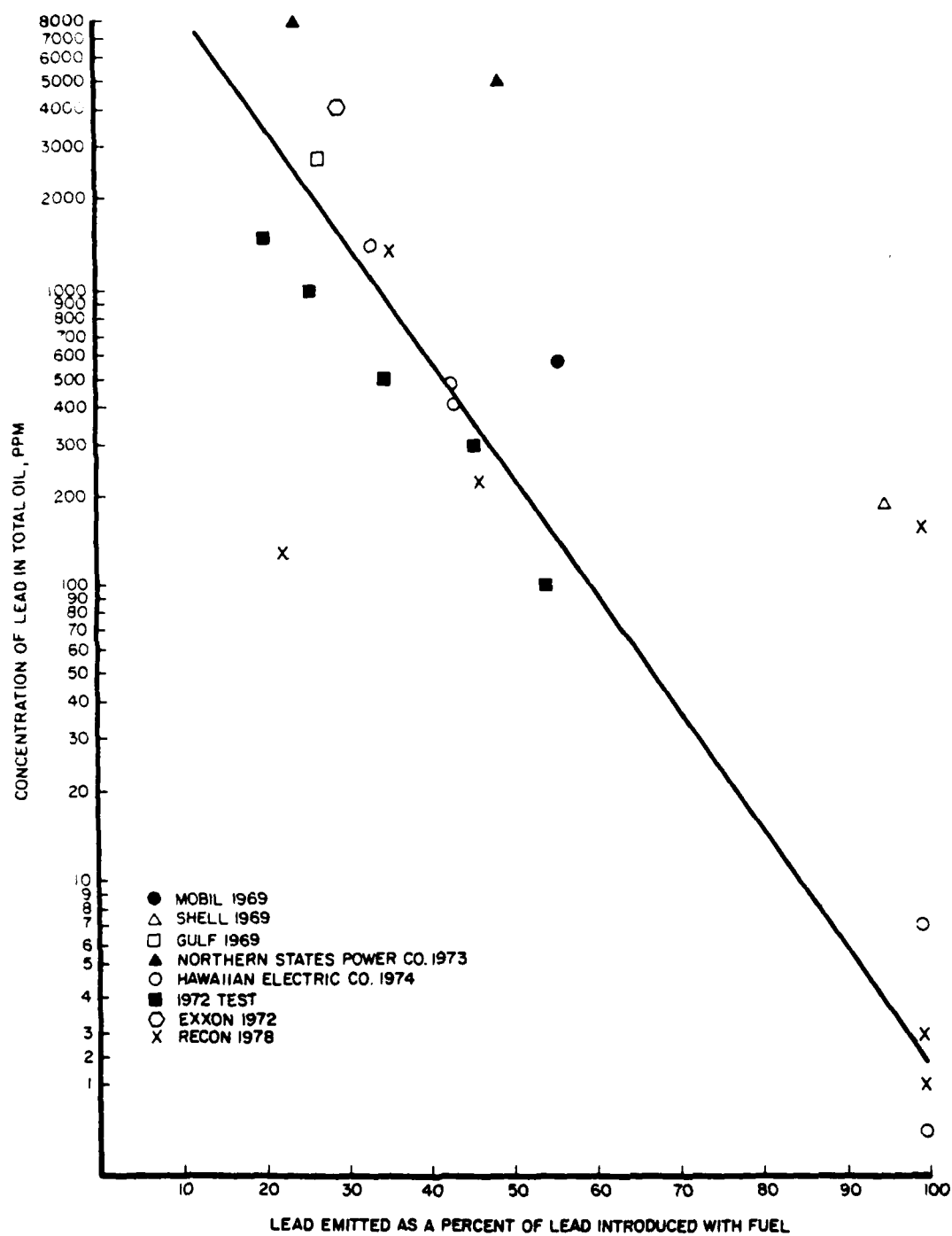


Figure C4. Lead emissions. (From *Used Oil Burned as a Fuel*, Vol 1, SW 892 [EPA, 1980].)

**Table C3**  
**Particle Size Distribution of Lead and Other Major Contaminants**  
**in Emissions from Waste Oil Combustion**

(From G. J. Mascetti and H. M. White, *Utilization of Used Oils*, Final Report, U.S. Department of Energy Contract EY-76-CO-3-1101 003/ATR7873841 [August 1978], p. 10-15)

| Particle Size  | Lead       | Calcium  | Weight Percent |            | Iron      | Barium    |
|----------------|------------|----------|----------------|------------|-----------|-----------|
|                |            |          | Phosphorus     | Zinc       |           |           |
| < 1 micron     | 76 to 69   | 10 to 19 | 23 to 42       | 56 to 73   | 2.7 to 36 | 3.3 to 51 |
| 1 to 10 micron | 16 to 21   | 71 to 74 | 49 to 66       | 23 to 39   | 51 to 80  | 49 to 79  |
| > 10 micron    | 2.7 to 4.4 | 10 to 15 | 8.9 to 10      | 3.4 to 5.0 | 13 to 18  | 8.9 to 18 |

EPA tests show that from 20 to 100 percent of the lead entering a steam boiler can be expected to be emitted from the stack. Some lead is emitted as an aerosol or vapor, though most is associated with particulates.<sup>55</sup> Table C3 lists the particle size distribution of lead and other major contaminants in emissions from waste oil combustion. Knowing particulate size is important for considering environmental and health effects of pollutants. Smaller particles penetrate deep into the human respiratory tract, whereas larger particulates tend to be removed in the upper tract.<sup>56</sup> Also, if pollution equipment is to be installed, the particle size distribution is an important design parameter.

In one EPA test, 90 percent of the lead emitted was associated with particulates smaller than 1 micron. Nearly 75 percent of this lead was recovered from boiler tubes, and 25 percent was emitted directly into the atmosphere. Furnace deposits may be emitted to the atmosphere during soot blowing, or may be removed during furnace cleaning.<sup>57</sup>

#### Other Pollutants

SO<sub>x</sub> emissions are a function of the sulfur content of the used oil. Since used crankcase oil usually has little sulfur, a blend of high sulfur residual oil and used oil can actually reduce SO<sub>x</sub> emissions and corrosion of internal boiler surfaces.<sup>58</sup>

<sup>55</sup> *Used Oil Burned as a Fuel*, p 4-4.

<sup>56</sup> H. C. Perkins, *Air Pollution* (McGraw-Hill, Inc., 1974), p 336.

<sup>57</sup> *Used Oil Burned as a Fuel*, p 4-3.

<sup>58</sup> P. D. Spawn and P. E. Fennelly, "An Updated Look at the Fuel Potential of Waste Automotive Oil," *Proceedings of a Workshop on Measurements and Standards for Recycled Oil-II*, Gaithersburg, Maryland, National Bureau of Standards, 1977 (NBS Special Publication 556, 1979), p 51.

SO<sub>x</sub> emissions will not be dealt with in this report because they are not specific to used oil combustion. Similarly, NO<sub>x</sub> emissions are a function of combustion temperature and the nitrogen in the oil, rather than being related to oil contamination.<sup>59</sup>

In *Used Oil Burned as a Fuel*, the EPA combines air pollution and used oil composition criteria to characterize a used oil which may be burned with minimal environmental risk. The results are presented in Table 8. In the same publication, the EPA suggests uncontrolled emission factors for used oil and used oil-virgin oil blends. The emission factors are consistent with those previously published for the selected pollutants (Table C4).<sup>60</sup>

#### Modeling

Before building storage facilities and modifying boilers to burn oil, it might be useful to model the lead emissions that would result from burning used oil. The model could help in calculating the maximum lead concentration allowable in the oil. This maximum depends on the ambient lead concentration before the boiler emissions' contribution, and on the lead emitted as a function of lead concentration in the fuel. The amount of lead could be reduced, then, either by pretreatment or by reducing the ratio of used oil to virgin fuel. Waste oil managers may contact CERL for information about the modeling procedure.

#### Pretreatment

Pretreatment of the used oil can significantly improve oil quality, thereby reducing boiler damage.

<sup>59</sup> J. T. Beard, F. A. Lachetta, and L. U. Lilleht, *Air Pollution Training Institute Course 427, Student Manual*, EPA 450/2-80-063 (EPA, February 1980), p 8-3.

<sup>60</sup> *Used Oil Burned as a Fuel*, p 4-4.

**Table C4**  
**Uncontrolled Emission Factors for Combustion**

(From *Used Oil Burned as a Fuel*, Vol 1, SW 892 [EPA, 1980])

| Emission Factors, lb/10 <sup>3</sup> gal       |   | Suggested<br>for Used Oil* | Comments   |
|--|---|----------------------------|--|
| Pollutant                                      | EPA AP-42 (3)   |                            |  |
| Pb   | Waste oil 0.0075(L)   | 0.0075(L)                  | L = ppm Pb in oil. Based on 100% emission at 7.5 lbs/gal oil density.  |
| Pb   | Virgin oils 0.0042(L)<br>(residual, distillate)   |                            | Based on substantially less than 100% emissions. Avg L = 1.0 for residual oils, and 0.1 for distillate oils.   |
|  | Coal 1.6(l) lb/10 <sup>3</sup> ton<br>(bituminous, anthracite)  | ---                        | Based on 80% emissions.  |
| Particulate                                    | Waste oil 75(A)   | 75(A)                      | A = % ash in oil. Based on 100% equivalent emission at 7.5 lbs/gal oil density.  |
| Particulate                                    | Virgin oils<br>#6 - 10(S) + 3<br>#5 - 10<br>#4 - 7<br>Ind./comm. dist. 2<br>Domestic dist. 2.5  |                            | S = % sulfur in oil.<br>Note that used oil with approx. 0.13% ash would be equivalent to #5 fuel oil.  |
| Other metals<br>in particulate                 | Not included  | 0.0075(L)                  | L = ppm metal in oil.  |
| SO <sub>2</sub>                                | Residual oil 157(S)<br>Distillate oil 142(S)  | 150(S)                     | S = % sulfur in oil. Suggested factor for used oil based on 100% conversion of S to SO <sub>2</sub> for 7.5 lb/gal oil density.  |
| SO <sub>x</sub>                                | All virgin oils - 2S  | 2S                         | S = % sulfur in oil.   |
| NO <sub>x</sub> (total<br>as NO <sub>2</sub> ) | Residual oils:<br>Power plant<br>tangential - 50<br>Power plant<br>other - 105<br>Ind./comm. 22+400(N)2<br>Ind./comm. dist. 22<br>Domestic dist. 18 | 22                         | N = % nitrogen in oil.<br>See AP-42 1.3 for further discussion of NO <sub>x</sub> emissions.   |
| Hydrocarbons<br>(total, as CH <sub>4</sub> )   | All virgin oils - 1   | 1                          | RECON measurements ranged from 14 to 165 µg/g fuel (113 avg) as compared to 1 lb/10 <sup>3</sup> gal (approx. 133 µg/g) emission factor.   |
| PNA's**  | Not included  | 0.0075                     | Corresponds to 1 µg/g. Insufficient data to determine how PNA emissions for used oils compare to virgin oils.  |
| HCl**  | Not included  | 77(C) max.                 | C = % chlorine in oil.   |
| HBr**  | Not included  | 76(B) max.                 | B = % bromine in oil.  |
| P (in<br>particulate)                          | Not included  | 75(P) max.                 | P = % phosphorous in oil.  |
| CO   | 5   | 5                          | CO emissions vary with combustion control on all fuels. No CO emission detected by Orsat analyses in RECON tests 1-4. Determinations by Kitagawa detector tube in runs 5-9 showed 10 to 100 ppm in the flue gas or an average of about 5 lb/10 <sup>3</sup> gal. |

\* And for used oil/virgin oil mixture.

\*\*Suggested for these pollutants.

over an extended time. The treatment may be as simple as screening to remove large foreign objects and sediment. The most common treatment is settling to remove water and sediment. More sophisticated reprocessing consists of centrifugation, filtration, atmospheric or vacuum distillation, or chemical treatment.<sup>61</sup>

## GLOSSARY

**additive:** A chemical added to improve oil.

**aniline number (or point):** Temperature (°C) at which mixtures of petroleum and aniline become miscible. The value is a measure of sludge solvent power. A low aniline number indicates high solvent power.

**asphalt:** A solid hydrocarbon found as a natural deposit. When subjected to distillation to remove light fractions, crude oil of high asphaltic content leaves asphalt as a residue. Asphalt is dark brown or black and is a solid at normal temperatures.

**BS&W:** Abbreviation for bottom solids and water. Found in petroleum crudes, undistilled fuels and used oils.

**flash point:** Maximum temperature at which oil can be stored and handled without serious fire hazard.

**lubricating oil:** That fraction of the crude oil which is sold to reduce friction in any industrial or mechanical application. This term includes re-refined oil.

**neutralization number:** The number of milligrams of potassium hydroxide needed to neutralize 1.0 g of an oil sample.

**pour point:** Primary indication of the lowest temperature at which an oil can be stored and still flow under very low forces.

**reclaiming or reprocessing:** Physical treatment with or without chemical treatment to prepare fuels from used oils.

**recycled oil:** Any used oil which is reused for any purpose. This includes oil which is re-refined, reclaimed, burned, or reprocessed.

**re-refined oil:** Used oil from which the physical and chemical contaminants acquired through use have been removed by a re-refining process.

**Saybolt Universal Viscosity:** Time (in seconds) it takes to run 60 mL of a fluid through a standard size orifice. Usually reported at 100°F, 150°F, or 210°F.

**Saybolt Furol Viscosity:** Same as Saybolt Universal Viscosity, except the orifice through which the fluid passes is larger; 62 seconds. Saybolt Furol Seconds (SFS) = 600 seconds SUS.

**used oil:** Any oil which has been refined from crude oil and used, and which has therefore been physically or chemically contaminated.

**virgin oil:** Oil products manufactured from previously unused petroleum products.

**viscosity:** Measure of a fluid's resistance to shear or angular deformation. Indicates relative ease of flow.

**viscosity index:** An empirical measure of the effect of temperature on the viscosity of oils. A low index indicates a large change with temperature.

## METRIC CONVERSIONS

1 gal = 3.785 L

°C = 5/9 (°F-32)

1 lb = 0.37 kg

1 psi = 6.895 × 10<sup>3</sup> Pa

1 Btu = 0.293 W

1 ton = 0.9 MT

1 mi = 1.6 km

1 in. = 25.4 mm

<sup>61</sup> *Used Oil Burned as a Fuel*, Vol 1, SW 892 (EPA, 1980), pp 2-6, 2-7.



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